

Contractor Name: Weirich, Carl

License Number: CVC56880

Address:

Phone Number:

City of Belle Isle

Universal Engineering Sciences 3532 Maggie Blvd., Orlando, FL 32811 Tel 407-581-8161 * Fax 407-581-0313 * www.universalengineering.com

PERMIT CARD – PLEASE POST AT JOB SITE

THIS DOCUMENT BECOMES YOUR PERMIT WHEN PROPERLY VALIDATED

Per FBC 105.3.3: An enforcing authority may not issue a building permit for any building construction, erection, alteration, modification, repair or addition unless the permit either includes on its face or there is attached to the permit the following statement: "NOTICE: In addition to the requirements of this permit, there may be additional restrictions applicable to this property that may be found in the public records of this county, and there may be additional permits required from other governmental entities such as water management districts, state agencies, or federal agencies." The issuance of this permit does not grant permission to violate any applicable City, Orange County, State of Florida and/or Federal codes and/or ordinances. Separate permits are required for Signs, Roofing, Electrical, Gas, Plumbing and Mechanical services. This permit becomes VOID if the work authorized is not commenced within 6 months, or is suspended or abandoned for a period of 6 months after commencement. WORK SHALL BE CONSIDERED SUSPENDED IF AN APPROVED INSPECTION HAS NOT BEEN MADE WITHIN A 6 MONTH PERIOD. PERMISSION IS GRANTED TO DO THE FOLLOWING WORK ACCORDING TO THE CONDITIONS HEREON AND THE APPROVED PLANS AND SPECIFICATIONS, SUBJECT TO

COMPLIANCE WITH THE ORDINANCES OF THE CITY OF BELLE ISLE, FLORIDA ELECTRICAL: Solar for electricity Scope of Work: Permit Number: 2015-04-017 Comments: None Date of Application: 04/07/2015 Date Permit Issued: 04/09/2015 **Project Information** Address: 1307 E. Wallace Street, Belle Isle, FL 32809 WARNING TO OWNER: "YOUR FAILURE TO RECORD A Parcel ID: 24-23-29-3400-00-078 Property Owner: Hafley, Michael & Patricia PAYING Phone Number: None ************************* Solar-Ray Inc Company Name:

NOTICE OF COMMENCEMENT MAY RESULT IN YOU TWICE FOR IMPROVEMENTS TO YOUR PROPERTY: IF YOU INTEND TO OBTAIN FINANCING, CONSULT WITH YOUR LENDER OR AN ATTORNEY RECORDING YOUR NOTICE COMMENCEMENT." ON THE JOB INSPECTION(S) MUST BE MADE BEFORE PROCEEDING WITH SUBSEQUENT WORK. THIS CARD MUST BE DISPLAYED OUTSIDE AND BE PROTECTED FROM THE WEATHER WHILE BEING VISIBLE FROM THE STREET UNTIL THE FINAL INSPECTIONS HAVE BEEN APPROVED.

6007 Anno Ave, Orlando, FL 32809

407-443-4404

100000	BUILDING FEATURES
IMPACT FEES	BUILDING INSPECTOR USE ONLY
School \$ Traffic \$	IF APPLICABLE: Have Zoning Approval Conditions Been Met? YES NO Have Stormwater Approval Conditions
ZONING FEES Zoning Fee \$	Been Met? YES NO Silt fencing in place? YES NO Turbidity Barrier in place? YES NO
UNIVERSAL ENG - BUILDING FEES	BUILDING 1 st (Footing/Foundation)
Cert of Occ \$	Survey specific foundation plan must be onsite before slab pour. Approved Plan on Site?
Demo \$ Building \$	2 nd (Slab)
Fence \$ Driveway \$	3 rd (Lintel)(Wall Reinforcing on Masonry Building)
Shed \$ Window(s) \$	4 th (Exterior Framing)(Roof/Wall Sheathing)
Door(s) \$ PrePower \$ Electrical \$295.50	5 th (Framing) (To be made after Plumbing/ Mechanical/ Electrical Rough-Ins & Windows/Doors Installed)
Temp Pole \$ Plumbing \$ Mechanical \$	6 th (Insulation to be Made After Roof Installed)
Gas \$ Roofing \$	7 th (Drywall)
Boat Dock \$ Screen Encl \$	8 th (Sidewalk/Driveway)
Swimming Pool \$ Sign \$	9 th (Other)
SURCHARGE FEES	10 th (Final – After MEP and Other Applicable Finals)
Surcharge Fee \$4.43 Surcharge Fee \$4.43	ROOFING 1 ST ROOFING Deck Nailing/Dry-in/Flashing
TOTAL FEES \$204.26	2 nd ROOFING Covering In-Progress
TOTAL FEES \$304.36	3 rd ROOFING Covering Final
Date Paid 4-17-15 Cor Check # WSA 8271	PLUMBING (Pool-Piping, Solar, Irrigation, Water Treatment Equip, Etc)
Cor Check # VSA 8071	1 ST (Underground) 2 nd (Sewer)
Amount Paid 304-36	3 rd (Rough-In/Tub Set) 4 th (Final)
The person accepting this permit shall conform to the terms of the application on file and construction shall conform to the requirements of the Florida Building Code (FS 553).	CHECK APPROPRIATE BOX GASNaturalLP

Inspection requests are to be emailed to BIDscheduling@UniversalEngineering.com; a confirmation email will be sent back to you upon scheduling. Next-Day Inspection requests must be made by 1pm. Please include the following in your request: Permit #, project address, type of inspection, date of the requested inspection, a contact name & a contact phone number. AM or PM may be requested but cannot be guaranteed.

TASK NUMBER \\ \B

CTTY OF BELLE ISLE

Permit Application Review Sheet

Permit Number	2015-04-017
Property Owner	HAFLEY
Address	1307 E. Wallace St.
Nature of Improvement	Solar: for electricity
Received Application	4-7-15
Sent for Stormwater Review	
Stormwater Approved	
Sent for Zoning Review	
Zoning Approved	
Applied for Variance	Contracts (Contract Contract) (Although Representations the entraction of the first in the first of the first
Variance Approved	
Sent to BO for Review	VL-7-15
Building Official Approved	4-8-15 84
	Comments
Susan 47-15	veren wo# 49293
2. Sotiti	Wester Wot 49293
3. 4-7-15 RU	NEED GOLAR PANEL ATTACHMENT
4.	DETAILS PREPARED BY A FLORIDA
5.	DESIGN PROFESSIONAL. ALSO NEED
6.	CUT SHEETS FOR INVERTER + ASSOCIATED
7.	ELECTRICAL EQUIP.
3. Sun 4715	emailed above comments
C 20 48-0	See who that arrived wo 49315
Susan 49-15	war I so givent investigation NEGATIVE
11.	no duble bels- emailed permet ready
"procenage of or	leck in person permet typed



PILS. TIS VIII

City of Belle Isle
Universal Engineering Sciences 3532 Maggie Blvd., Orlando, FL 32811
Tel 407-581-8161 * Fax 407-581-0313 * www.universalengineering.com

APPLICATION FOR ELECTRICAL PERMIT

WARNING TO OWNER: YOUR FAILURE TO RECORD A NOTICE OF COMMENCEMENT MAY RESULT IN YOUR PAYING TWICE FOR IMPROVEMENTS TO YOUR PROPERTY. A NOTICE OF COMMENCEMENT MUST BE RECORDED AND POSTED ON THE JOB SITE BEFORE THE FIRST INSPECTION. IF YOU INTEND TO OBTAIN FINANCING, CONSULT WITH YOUR LENDER OR AN ATTORNEY BEFORE RECORDING YOUR NOTICE OF COMMENCEMENT.

DATE OF APPLICATION: April 6, 201 The undersigned hereby applies for a per	mit to make electrical	PER I installations as indicate	MIT NUMBER Id below. PLEASE	2015-04-0
Project Address 1307 E. Wallace S	t		, Belle (sie FL	✓ 32809 □ 32812
Property Owner Michael & Patricia	Hafley		Phone	'-687-2518
Property Owner's Mailing Address 1307			City_Belle I	sle
State Florida Zip Code 32809				z/Searches/ParcelSearch.aspx
Class of Building: Old New Type of Work: New Alteration	Type of Building	: Residentis ☑ Con	_	Other Existing
INDICATE	THE QUANTITY O	F ALL EQUIPMENT TO		
Dishwasher Exhaust Fan				er Heater
Hood Fan Dryer		Paddie Fan	Outle	sta
Fixtures Spa		Pool	Switc	hes
Electric Signs Meter Reset _		Low Voltage		8
Pumps Motors		_Air Conditioning (tons)	Fum	ace (KW)
Temporary Construction Pole	One (1)	New <u>Mater</u> Service		Amperage/Voltage/Phase
Meter Service Upgrade from		to	_	
	/Voltage/Phase	Amperage/Voltage	/Dhose F	Difference in Size
Other: Attach solar photovoltaic PERMIT FEE BASED ON METER SEI (IF NO METER SERVICE WORK BEIN VALUATION OF JOB (VALUATION O	RVICE SIZE SCHED NG DONE, USE VAL	ULE . UATION OF JOB FOR I	. \$ PERMIT FEE)	
(A)		99	\neg	R Fee = \$ 197.00
Building Official:		4-8-15	5	w Fee = \$ 1800
Verified Contractor's Licenses & Insurar	nce are on file	Date 4-7-1	2	Surcharge = \$
				L Permit = \$
I hereby certify that the above is true and of the hereby make Application for Permit as outline Ordinances regulating same and in accordance applicable Town and/or State of Florida codes	ed above, and if same i	s granted agree to confo	rm to all Florida Buil nit does not grant po LICENSE # C	ermission to violate any
LICENSE HOLDER SIGNATURE	VVV	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	LICENSE #	¥C 30080
LICENSE HOLDER NAME Carl Weiric Street Address 6007 Anno Ave	<u>n</u>	COMPANY NA	Solar-Ray	y Inc.
Ordendo		00000		10T 110 100 1
City Orlando Email Address Carl@solar-ray.net	State FL	Zip Code 32809	Phone Numbe	407-443-4404
NOTE: The Building Permit Number is requir Permit has been issued.	ed if the Electrical Inst	aliation is associated with	any construction or	alteration where a Building



COBI Permit Fee Calculation Form



Reviewer Signature:	7	Date:
Permit Type:	ELECTRICAL	Job Cost: \$ 32,300
Permit Fee:	\$ 197,00	98.50
Plans Review Fee:	\$ 98.50	(50% of permit fee – excluding ReRoofs)
1.5% State Fee:	<u>\$ 4.43</u>	4.43
1.5% State Fee:	s <u>4.43</u>	8.86
TOTAL BUILDING FEE:	\$ 304.36 Note: Total gets doubled for	(does not include Zoning fees or Deposits) SvvO/AFT permits
1 ⁵ 10	000 = 37.00	

15 1000 = 37.00 5.00 / APORTIONAL 1000 ORFRACTION 32 X5 = 160.00 160.00 + 37 = [197.00 PERMIT 197:2 = 98.50 REUIEW] 2955 x 0.015 4,43 1.5% SURCHARGE 197.00 + 98.50 + 4.43 + 4.43 = 304.36 TOTAL

Permit Number: Folio/Parcel ID #: 24-23-29-3400-00-078 Prepared by: Solze-Regular Confidence Return to: Solze-Begular Confidence Return to: Solze-Begular Confidence Return to Due Confidence Results Confi	DOC# 20150170069 B: 10899 P: 873 04/07/2015 12:05:58 PM Page 1 of 1 Rec Fee: \$10.00 Martha O. Haynie, Comptroller Orange County, FL MB - Ret To: SOLAR RAY INC
NOTICE OF COMMENCEMENT State of Florida, County of Orange The undersigned hereby gives notice that improvement will be made with Chapter 713, Florida Statutes, the following information is provided in the property (legal description of the property, and some standard was a context of the property of	Telephone Number 402443-4404
Name And Address Lender Name And Address Lender Name And Address Persons within the State of Florida designated by Owner up	Telephone Number Amount of Bond \$ Telephone Number
be served as provided by §713.13(1)(a)7, Florida Statutes. Name NR Address In addition to himself or herself, Owner designates the folio Notice as provided in §713.13(1)(b), Florida Statutes. Name NR Address Expiration date of notice of commencement (the expiration dunless a different date is specified) AGE 30, 2015	Telephone Number wing to receive a copy of the Lienor's Telephone Number
NG TO OWNER: ANY PAYMENTS MADE BY THE OWNER AFTER THE EXPIR INSIDERED IMPROPER PAYMENTS UNDER CHAPTER 713, PART I, SECTION IN YOUR PAYING TWICE FOR IMPROVEMENTS TO YOUR PROPERTY. A NOT DED AND POSTED ON THE JOB SITE BEFORE THE FIRST INSPECTION. IF YOUR LENDER OR AN ATTORNEY BEFORE COMMENCING WORK OR RECORD TO THE FORMAL OF THE SECOND THE YOUR LENDER OR AN ATTORNEY BEFORE COMMENCING WORK OR RECORD TO THE YOUR PROPERTY. A NOT THE YOUR PROPERTY.	TATALLA STATUTES, AND CAN OTICE OF COMMENCEMENT MUST BE YOU INTEND TO OBTAIN FINANCING, CONSULT RDING YOUR NOTICE OF COMMENCEMENT. Manager Signatory's Title/Office OUT 16 Dy Potricia Haffey month/year name of person Try on behalf of whom instrument was executed JANERY FRUTO Commission # FF 142524 For stamp commissioned mane of lotary Public
	repared by: \$124-13-29-3400-00-074 repared by: \$124-13-29-3400-00-074 repared by: \$124-13-29-3400-00-074 repared by: \$124-13-13-13(1)(a)7, Florida Statutes. NOTICE OF COMMENCEMENT tate of Florida designated by Owner up be served as provided in \$713.13(1)(b), Florida Statutes. NOTICE OF COMMENCEMENT tate of Florida designated by Owner up be served as provided in \$713.13(1)(b), Florida Statutes. NOTICE OF COMMENCEMENT to the more served as provided in \$713.13(1)(b), Florida Statutes. NOTICE OF COMMENCEMENT to the more served as provided in \$713.13(1)(b), Florida Statutes. Name Petron Hame Statutes. Name Petron Hame Statutes. Name Statutes. Name Statutes. Name Statutes. Name Address Contractor Name Statutes. Name Address Lender Name Address Lender Address Lender Name Addre

Form content revised: 01/23/14



Code-Compliant Installation Manual 227.3
For ASCE 7-05 or ASCE 7-10

U.S. Des. Patent No. D496,248S, D496,249S. Other patents pending.



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i. Installer's Responsibilities

Please review this manual thoroughly before installing your SOLARMOUNT system.

This manual provides (1) supporting documentation for building permit applications relating to Unirac's SOLARMOUNT Universal PV Module Mounting system, and (2) planning and assembly instructions for SOLARMOUNT

SOLARMOUNT products, when installed in accordance with this bulletin, will be structurally adequate and will meet the structural requirements of the IBC 2009 and IBC 2012, ASCE 7-05, ASCE 7-10 and California Building Code 2013 (collectively referred to as "the Code").

SOLARMOUNT is much more than a product.

It's a system of engineered components that can be assembled into a wide variety of PV mounting structures. With SOLARMOUNT you'll be able to solve virtually any PV module mounting challenge.

It's also a system of technical support: complete installation and code compliance documentation, an on-line SOLARMOUNT Estimator, person-to-person customer service, and design assistance to help you solve the toughest challenges.

This is why SOLARMOUNT is PV's most widely used mounting system.



The installer is solely responsible for:

- Complying with all applicable local or national building codes, including any that may supersede this manual;
- Ensuring that Unirac and other products are appropriate for the particular installation and the installation environment;
- Ensuring that the roof, its rafters, connections, and other structural support members can support the array under all code level loading conditions (this total building assembly is referred to as the building structure);
- Using only Unirac parts and installer-supplied parts as specified by Unirac (substitution of parts may void the warranty and invalidate the letters of certification in all Unirac publications);
- Ensuring that lag screws have adequate pullout strength and shear capacities as installed;
- Verifying the strength of any alternate mounting used in lieu of the lag screws;
- Maintaining the waterproof integrity of the roof, including selection of appropriate flashing;
- Ensuring safe installation of all electrical aspects of the PV array;
- Ensuring correct and appropriate design parameters are used in determining the design loading used for design of the specific installation. Parameters, such as snow loading, wind speed, exposure and topographic factor should be confirmed with the local building official or a licensed professional engineer.





NOTE - If you have run our U-Builder at www.design.unirac.com/tool/project_info/solarmount/?pitched=true turn to page 29 for installation instructions.

Part I. Procedure to Determine the Design Wind Load

[1.1.1.] Using the Simplified Method - ASCE 7-05

The procedure to determine Design Wind Load is specified by the American Society of Civil Engineers and referenced in the International Building Code 2009. For purposes of this document, the values, equations and procedures used in this document reference ASCE 7-05, Minimum Design Loads for Buildings and Other Structures. *Please refer to ASCE 7-05 if you have any questions about the definitions or procedures presented in this manual.* Unirac uses Method 1, the Simplified Method, for calculating the Design Wind Load for pressures on components and cladding in this document.

The method described in this document is valid for flush, no tilt, SOLARMOUNT Series applications on either roofs or walls. Flush is defined as panels parallel to the surface (or with no more than 3" difference between ends of assembly) with no more than 10" space between the roof surface, and the bottom of the PV panels.

This method is not approved for open structure calculations. *Applications of these procedures is subject to the following ASCE 7-05 limitations:*

- 1. The building height must be less than 60 feet, h < 60. See note for determining h in the next section. For installations on structures greater than 60 feet, contact your local design professional.
- 2. The building must be enclosed, not an open or partially enclosed structure, for example a carport.
- 3. The building is regular shaped with no unusual geometrical irregularity in spatial form, for example a geodesic dome.
- 4. The building is not in an extreme geographic location such as a narrow canyon or steep cliff.
- 5. The building has a flat or gable roof with a pitch less than 45 degrees or a hip roof with a pitch less than 27 degrees.
- 6. If your installation does not conform to these requirements please contact your local Unirac distributor or a local professional engineer.

If your installation is outside the United States or does not meet all of these limitations, consult a local professional engineer or your local building authority. Consult ASCE 7-05 for more clarification on the use of Method I. Lower design

wind loads may be obtained by applying Method II from ASCE 7-05. Consult with a licensed engineer if you want to use Method II procedures.

The equation for determining the Design Wind Load for components and cladding is:

 $p_{net}(psf) = \lambda K_{zt} I p_{net30}$

 $p_{net}(psf) = Design Wind Load$

 λ = adjustment factor for building height and exposure category

 $K_{zt} = Topographic Factor at mean roof height, h (ft)$

I = Importance Factor

 p_{net30} (psf) = net design wind pressure for Exposure B, at height = 30 feet, I = 1.0

You will also need to know the following information:

Basic Wind Speed = V (mph), the largest 3 second gust of wind in the last 50 years.

 $h\left(ft\right)=total\ roof\ height\ for\ flat\ roof\ buildings\ or\ mean\ roof\ height\ for\ pitched\ roof\ buildings$

Roof Pitch (degrees)

This manual will help you determine:

Effective Wind Area (sf) = minimum total continuous area of modules being installed (Step 2)

 $Roof\ Zone = the\ area\ of\ the\ roof\ you\ are\ installing\ the\ pv\ system$ according to $Step\ 3$.

Roof Zone Dimension = a (ft) (Step 3)

Exposure Category (Step 6)

[1.1.2.] Using the Low Rise Buildings (Simplified) - ASCE 7-10

The procedure to determine Design Wind Load is specified by the American Society of Civil Engineers and referenced in the International Building Code 2012 and California Building Code 2013. For purposes of this document, the values, equations and procedures used in this document reference ASCE 7-10, Minimum Design Loads for Buildings and Other Structures. *Please refer to ASCE 7-10 if you have any questions about the definitions or procedures presented in this manual.* Unirac uses Part 2, The Simplified Method, for low rise buildings to calculate the Design Wind Load for pressures on components and cladding in this document.

The method described in this document is valid for flush,

no tilt, SOLARMOUNT Series applications on either roofs or walls. Flush is defined as panels parallel to the surface (or with no more than 3" difference between ends of assembly) with no more than 10" space between the roof surface, and the bottom of the PV panels.

This method is not approved for open structure calculations. Applications of these procedures is subject to the following ASCE 7-10 limitations:

1. The building height must be less than 60 feet, h < 60. See note for determining h in the next section. For installations on structures greater than 60 feet, contact your local design professional. Reviewed for Code Compliance 3

- 2. The building must be enclosed, not an open or partially enclosed structure, for example a carport.
- 3. The building is regular shaped with no unusual geometrical irregularity in spatial form, for example a geodesic dome.
- 4. The building is not in an extreme geographic location such as a narrow canyon or steep cliff.
- 5. The building has a flat or gable roof with a pitch less than 45 degrees or a hip roof with a pitch less than 27 degrees.
- 6. If your installation does not conform to these requirements please contact your local professional engineer.

If your installation is outside the United States or does not meet all of these limitations, consult a local professional engineer or your local building authority. Consult ASCE 7-10 for more clarification on the use of Part 2.

The equation for determining the Design Wind Load for components and cladding is:

 $p_{net}(psf) = \lambda K_{zt} p_{net30}$

 $p_{net}(psf) = Design Wind Load$

 λ = adjustment factor for building height and exposure category

 $K_{zt} = Topographic Factor = 1$

 p_{net30} (psf) = net design wind pressure for Exposure B, at height = 30 feet

You will also need to know the following information:

Basic Wind Speed = V (mph), the largest 3 second gust of wind in the last 50 years.

 $h(ft) = total\ roof\ height\ for\ flat\ roof\ buildings\ or\ mean\ roof\ height\ for\ pitched\ roof\ buildings$

Roof Pitch (degrees)

This manual will help you determine:

Effective Wind Area (sf) = minimum total continuous area of modules being installed (Step 2)

Roof Zone = the area of the roof you are installing the pv system according to Step 3.

Roof Zone Dimension = a (ft) (Step 3)

Exposure Category (Step 6)

[1.2.1.] Procedure to Calculate Total Design Wind per ASCE 7-05

See page 11 for ASCE 7-10 procedure.

The procedure for determining the Design Wind Load can be broken into steps that include looking up several values in different tables. Table 5 has been provided as a worksheet for the following 9 steps (page 9)

Step 1: Determine Basic Wind Speed, V (mph)

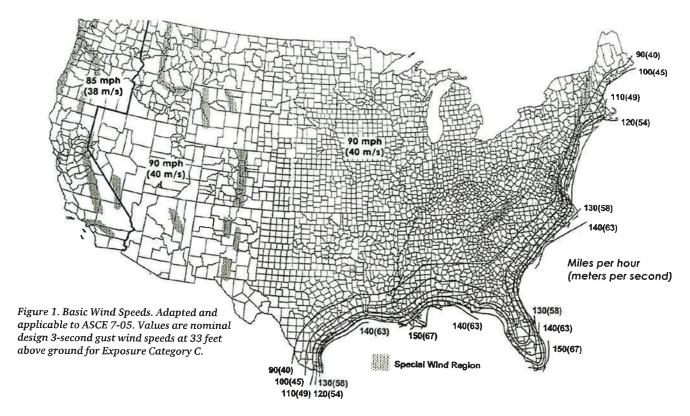
Determine the *Basic Wind Speed, V (mph)* by consulting your local building department or locating your installation on the maps in Figure 1, page 5.

Step 2: Determining Effective Wind Area

Determine the smallest area of continuous modules you will be installing. This is the smallest area tributary (contributing load) to a support or to a simple-span of rail. That area is the Effective Wind Area, the total area of the fewest number of modules on a run of rails. If the smallest area of continuous modules exceeds 100 sq ft, use 100 sq ft (See Table 2). If less, round down to values available in Table 2.







ASCE 7-05.

Step 3: Determine Roof/Wall Zone

The Design Wind Load will vary based on where the installation is located on a roof. Arrays may be located in more than one roof zone.

Using Table 1, determine the Roof Zone Dimension Length, a (ft), according to the width and height of the building on which you are installing the pv system.



Table 1. Determine Roof/Wall Zone, dimension (a) according to building width and height

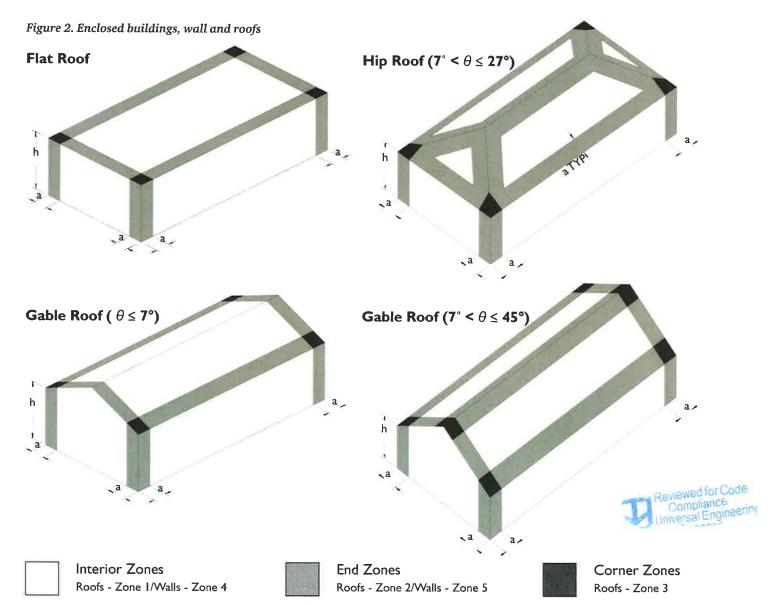
a = 10 percent of the least horizontal dimension or 0.4h, whichever is smaller, but not less than either 4% of the least horizontal dimension or 3 ft of the building.

Roof	Least Horizontal Dimension (ft)																		
Height (ft)	10	15	20	25	30	40	50	60	70	80	90	100	125	150	175	200	300	400	500
10	3	3	3	3	3	4	4 -	4	4	4	4	4	5	6	7	8	12	16	20
15	3	3	3	3	3	4	5	6	6	6	6	6	6	6	7	8	12	16	20
20	3	3	3	3	3	4	5	6	7	8	8	8	8	8	8	8	12	16	20
25	3	3	3	3	3	4	5	6	7	8	9	10	10	10	10	10	12	16	20
30	3	3	3	3	3	4	5	6	7	8	9	10	12	12	12	12	12	16	20
35	3	3	3	3	3	4	5	6	7	8	9	10	12.5	14	14	14	14	16	20
40	3	3	3	3	3	4	5	6	7	8	9	10	12.5	15	16	16	16	16	20
45	3	3	3	3	3	4	5	6	7	8	9	10	12.5	15	17.5	18	18	18	20
50	3	3	3	3	3	4	5	6	7	8	9	10	12.5	15	17.5	20	20	20	20
60	3	3	3	3	3	4	5	6	7	8	9	10	12.5	15	17.5	20	24	24	24

Source: ASCE/SEI 7-05, Minimum Design Loads for Buildings and Other Structures, Chapter 6, Figure 6-3, p. 41.

Step 3: Determine Roof Zone (continued)

Using *Roof Zone Dimension Length*, a, determine the roof zone locations according to your roof type, gable, hip or monoslope. Determine in which roof zone your pv system is located, Zone 1, 2, or 3 according to Figure 2.



Source: ASCE/SEI 7-05, Minimum Design Loads for Buildings and Other Structures, Chapter 6, $p.41_{\odot}$

ASCE 7-05

Step 4: Determine Net Design Wind Pressure, p_{net30} (psf)

Using the Effective Wind Area (Step 2), Roof Zone Location (Step 3), and Basic Wind Speed (Step 1), look up the appropriate Net Design Wind Pressure in Table 2, page 7. Use the Effective Wind Area value in the table which is smaller than the value calculated in Step 2. If the installation is located on a roof overhang, use Table 3, page 8.

Both downforce and uplift pressures must be considered in overall design. Refer to **Section II**, **Step 1** for applying downforce and uplift pressures. Positive values are acting toward the surface. Negative values are acting away from the surface.



Table 2. p_{net30} (psf) Roof and Wall

			Basic Wind Speed, V (mph)								
		E Ffortivo	90	100	110	120	130	140	150	170	
	Zone	Effective Wind Area	Davidson Hall	- D	Daniel Lieff	D6 11-86	D	December 11-16	D	Davidson Hall	
-	Zone	(sf)	Downforce Upli	t Downtorce Upint	Downforce Uplift	Downtorce Upint	Downtorce Uplitt	Downtorce Uplitt	Downtorce Uplift	Downtorce Opint	
	i	10	5.9 -14.6	7.3 -18.0	8.9 -21.8	10.5 -25.9	12.4 -30.4	14.3 -35.3	16.5 -40.5	21.1 -52.0	
	i	20	5.6 -14.2		8.3 -21.2	9.9 -25.2	11.6 -29.6	13.4 -34.4	15.4 -39.4	19.8 -50.7	
es	1	50	5.1 -13.7		7.6 -20.5	9.0 -24.4	10.6 -28.6	12.3 -33.2	14.1 -38.1	18.1 -48.9	
degrees	I.	100	4.7 -13.3	5.8 -16.5	7.0 -19.9	8.3 -23.7	9.8 -27.8	11.4 -32.3	13.0 -37.0	16.7 -47.6	
	2	10	5.9 -24.4	7.3 -30.2	8.9 -36.5	10.5 -43.5	12.4 -51.0	14.3 -59.2	16.5 -67.9	21.1 -87.2	
0.7	2	20	5.6 -21.8	6.9 -27.0	8.3 -32.6	9.9 -38.8	11.6 -45.6	13.4 -52.9	15.4 -60.7	19.8 -78.0	
0	2	50	5.1 -18.4		7.6 -27.5	9.0 -32.7	10.6 -38.4	12.3 -44.5	14.1 -51.1	18.1 -65.7	
Roof 0 to	2	100	4.7 -15.8	5.8 -19.5	7.0 -23.6	8.3 -28.1	9.8 -33.0	11.4 -38.2	13.0 -43.9	16.7 -56.4	
×	3	10	5.9 -36.8		8.9 -55.0	10.5 -65.4	12.4 -76.8	14.3 -89.0	16.5 -102.2		
	3	20	5.6 -30.5		8.3 -45.5	9.9 -54.2	11.6 -63.6	13.4 -73.8	15.4 -84.7	19.8 -108.7	
	3	50	5.1 -22.1	6.3 -27.3	7.6 -33.1	9.0 -39.3	10.6 -46.2	12.3 -53.5	14.1 -61.5	18.1 -78.9	
	3	100	4.7 -15.8	5.8 -19.5	7.0 -23.6	8.3 -28.1	9.8 -33.0	11.4 -38.2	13.0 -43.9	16.7 -56.4	
	ī	10	8.4 -13.3	10.4 -16.5	12.5 -19.9	14.9 -23.7	17.5 -27.8	20.3 -32.3	23.3 -37.0	30.0 -47.6	
	i	20	7.7 -13.0		11.4 -19.4	13.6 -23.0	16.0 -27.0	18.5 -31.4	21.3 -36.0	27.3 -46.3	
es	i	50	6.7 -12.5		10.0 -18.6	11.9 -22.2	13.9 -26.0	16.1 -30.2	18.5 -34.6	23.8 -44.5	
27degrees	1	100	5.9 -12.1	7.3 -14.9	8.9 -18.1	10.5 -21.5	12.4 -25.2	14.3 -29.3	16.5 -33.6	21.1 -43.2	
7de	2	10	8.4 -23.2	10.4 -28.7	12.5 -34.7	14.9 -41.3	17.5 -48.4	20.3 -56.2	23.3 -64.5	30.0 -82.8	
0 2	2	20	7.7 -21.4	9.4 -26.4	11.4 -31.9	13.6 -38.0	16.0 -44.6	18.5 -51.7	21.3 -59.3	27.3 -76.2	
7 t	2	50	6.7 -18.9		10.0 -28.2	11.9 -33.6	13.9 -39.4	16.1 -45.7	18.5 -52.5	23.8 -67.4	
Roof >7 to	2	100	5.9 -17.0	7.3 -21.0	8.9 -25.5	10.5 -30.3	12.4 -35.6	14.3 -41.2	16.5 -47.3	21.1 -60.8	
ě	3	10	8.4 -34.3		12.5 -51.3	14.9 -61.0	17.5 -71.6	20.3 -83.I	23.3 -95.4	30.0 -122.5	
-	3	20	7.7 -32.1		11.4 -47.9	13.6 -57.1	16.0 -67.0	18.5 -77.7	21.3 -89.2	27.3 -114.5	
	3	50 100	6.7 -29.1 5.9 -26.9		10.0 -43.5 8.9 -40.2	11.9 -51.8 10.5 -47.9	13.9 -60.8 12.4 -56.2	16.1 -70.5 14.3 -65.1	18.5 -81.0 16.5 -74.8	23.8 -104.0 21.1 -96.0	
	3	100	3.7 -20.7	7.3 -33.2	6.7 -40.2	10.3 -47.7	12.4 -30.2	14.3 -65.1	16.5 -74.8	21.1 -76.0	
	1	10	13.3 -14.6	16.5 -18.0	19.9 -21.8	23.7 -25.9	27.8 -30.4	32.3 -35.3	37.0 -40.5	47.6 -52.0	
١.	l î l	20	13.0 -13.8		19.4 -20.7	23.0 -24.6	27.0 -28.9	31.4 -33.5	36.0 -38.4	46.3 -49.3	
ees	1	50	12.5 -12.8	15.4 -15.9	18.6 -19.2	22.2 -22.8	26.0 -26.8	30.2 -31.1	34.6 -35.7	44.5 -45.8	
degrees	1	100	12.1 -12.1	14.9 -14.9	18.1 -18.1	21.5 -21.5	25.2 -25.2	29.3 -29.3	33.6 -33.6	43.2 -43.2	
Ď	2	10	13.3 -17.0	16.5 -21.0	19.9 -25.5	23.7 -30.3	27.8 -35.6	32.3 -41.2	37.0 -47.3	47.6 -60.8	
45	2	20	13.0 -16.3		19.4 -24.3	23.0 -29.0	27.0 -34.0	31.4 -39.4	36.0 -45.3	46.3 -58.1	
7 to	2	50	12.5 -15.3		18.6 -22.9	22.2 -27.2	26.0 -32.0	30.2 -37.1		44.5 -54.6	
2	2	100	12.1 -14.6	14.9 -18.0	18.1 -21.8	21.5 -25.9	25.2 -30.4	29.3 -35.3		43.2 -52.0	
Roof >27	3	10	13.3 -17.0		19.9 -25.5	23.7 -30.3	27.8 -35.6		37.0 -47.3	47.6 -60.8	
ĕ	3	20	13.0 -16.3		19.4 -24.3	23.0 -29.0	27.0 -34.0	31.4 -39.4 30.2 -37.1		46.3 -58.1 44.5 -54.6	
	3	50 100	12.5 -15.3 12.1 -14.6		18.6 -22.9 18.1 -21.8	22.2 -27.2 21.5 -25.9	26.0 -32.0 25.2 -30.4				
		1.00			21.0	25 25.7			10.0		
	4	10	14.6 -15.8	18.0 -19.5	21.8 -23.6	25.9 -28.1	30.4 -33.0	35.3 -38.2	40.5 -43.9	52.0 -56.4	
	4	20	13.9 -15.1	17.2 -18.7	20.8 -22.6	24.7 -26.9	29.0 -31.6	33.7 -36.7		49.6 -54.1	
	4	50	13.0 -14.3		19.5 -21.3	23.2 -25.4	27.2 -29.8	31.6 -34.6			
_	4	100	12.4 -13.6		18.5 -20.4	22.0 -24.2	25.9 -28.4				
Wall	4	500	10.9 -12.1		16.2 -18.1	19.3 -21.5	22.7 -25.2	26.3 -29.3			
	5	10	14.6 -19.5		21.8 -29.1	25.9 -34.7	30.4 -40.7	35.3 -47.2			
	5	20 50	13.9 -18.2 13.0 -16.5		20.8 -27.2 19.5 -24.6	24.7 -32.4 23.2 -29.3	29.0 -38.0 27.2 -34.3			49.6 -64.9 46.6 -58.7	
	5	100	12.4 -15.1		18.5 -22.6	22.0 -26.9	25.9 -31.6	30.0 -36.7			
	5	500	10.9 -12.1		16.2 -18.1	19.3 -21.5	22.7 -25.2	26.3 -29.3		38.8 -43.2	
										17-4 Pode	

Source: ASCE/SEI 7-05, Minimum Design Loads for Buildings and Other Structures, Chapter 6, Figure 6-3, p. 42-43.





Table 3. p_{net30} (psf) Roof Overhang

		Effective				Basic Wind Speed,	V (mph)			
	Zone	Wind Area (sf)	90	100	110	120	130	140	150	170
S	2	10	-21.0	-25.9	-31.4	-37.3	-43.8	-50.8	-58.3	-74.9
degrees	2	20	-20.6	-25.5	-30.8	-36.7	-43.0	-49.9	-57.3	-73.6
20	2	50	-20.1	-24.9	-30.1	-35.8	-42.0	-48.7	-55.9	-71.8
7 d	2	100	-19.8	-24.4	-29.5	-35.I	-41.2	-47.8	-54.9	-70.5
to	3	10	-34.6	-42.7	-51.6	-61.5	-72.1	-83.7	-96.0	-123.4
0	3	20	-27.1	-33.5	-40.5	-48.3	-56.6	-65.7	-75.4	-96.8
Roof	3	50	-17.3	-21.4	-25.9	-30.8	-36.1	-41.9	-48.1	-61.8
Ϋ́	3	100	-10.0	-12.2	-14.8	-17.6	-20.6	-23.9	-27.4	-35.2
es	2	10	-27.2	-33.5	-40.6	-48.3	-56.7	-65.7	-75.5	-96.9
ē	2	20	-27.2	-33.5	-40.6	-48.3	-56.7	-65.7	-75.5	-96.9
Jeg	2	50	-27.2	-33.5	-40.6	-48.3	-56.7	-65.7	-75.5	-96.9
27degrees	2	100	-27.2	-33.5	-40.6	-48.3	-56.7	-65.7	-75.5	-96.9
t	3	10	-45.7	-56.4	-68.3	-81.2	-95.3	-110.6	-126.9	-163.0
7	3	20	-41.2	-50.9	-61.6	-73.3	-86.0	-99.8	-114.5	-147.1
Roof	3	50	-35.3	-43.6	-52.8	-62.8	-73.7	-85.5	-98.1	-126.1
	3	100	-30.9	-38.1	-46.1	-54.9	-64.4	-74.7	-85.8	-110.1
45degrees	2	10	-24.7	-30.5	-36.9	-43.9	-51.5	-59.8	-68.6	-88. I
50	2	20	-24.0	-29.6	-35.8	-42.6	-50.0	-58.0	-66.5	-85.5
흥	2	50	-23.0	-28.4	-34.3	-40.8	-47.9	-55.6	-63.8	-82.0
	2	100	-22.2	-27.4	-33.2	-39.5	-46.4	-53.8	-61.7	-79.3
7 to	3	10	-24.7	-30.5	-36.9	-43.9	-51.5	-59.8	-68.6	-88. I
>27	3	20	-24.0	-29.6	-35.8	-42.6	-50.0	-58.0	-66.5	-85.5
Ç	3	50	-23.0	-28.4	-34.3	-40.8	-47.9	-55.6	-63.8	-82.0
Roof	3	100	-22.2	-27.4	-33.2	-39.5	-46.4	-53.8	-61.7	-79.3

Source: ASCE/SEI 7-05, Minimum Design Loads for Buildings and Other Structures, Chapter 6, p. 44.

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Step 5: Determine the Topographic Factor, K_{zt}

For the purposes of this code compliance document, the *Topographic Factor*, K_{zt} , is taken as equal to one (1), meaning, the installation is surrounded by level ground (less than 10% slope). If the installation is not surrounded by level ground, please consult ASCE 7-05, Section 6.5.7 and the local building authority to determine the *Topographic Factor*.

Step 6: Determine Exposure Category (B, C, D)

Determine the *Exposure Category* by using the following definitions for Surface Roughness Categories.

The ASCE/SEI 7-05 defines wind surface roughness categories as follows:

Surface Roughness B: is urban and suburban areas, wooded areas, or other terrain with numerous closely spaced obstructions having the size of single family dwellings.

Surface Roughness c: has open terrain with scattered obstructions having heights generally less than 30 feet. This category includes flat open country, grasslands, and all water surfaces in hurricane prone regions.

Surface Roughness D: has flat, unobstructed areas and water surfaces outside hurricane prone regions. This category includes smooth mud flats, salt flats, and unbroken ice.

Also see ASCE 7-05 pages 287-291 for further explanation and explanatory photographs, and confirm your selection with the local building authority.





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Step 7: Determine adjustment factor for height and exposure category, λ

Using the *Exposure Category* (**Step 6**) and the *roof height*, *h* (*ft*), look up the *adjustment factor for height and exposure* in **Table 4**.

Step 8: Determine the Importance Factor, I

Determine if the installation is in a hurricane prone region. Look up the *Importance Factor, I*, Table 6, page 10, using the occupancy category description and the hurricane prone region status.

Step 9: Calculate the Design Wind Load, p_{net} (psf)

Multiply the Net Design Wind Pressure, p_{net30} (psf) (Step 4) by the adjustment factor for height and exposure, λ (Step 7), the Topographic Factor, K_{zt} (Step 5), and the Importance Factor, I (Step 8) using the following equation, or Table 5 Worksheet.

$$p_{net}(psf) = \lambda K_{zt} I p_{net30}$$

 $p_{net}(psf) = Design Wind Load (10 psf minimum)$

 λ = adjustment factor for height and exposure category (Step 7)

 $K_{zt} = Topographic Factor at mean roof height, h (ft) (Step 5)$

I = Importance Factor (**Step 8**)

 p_{net30} (psf) = net design wind pressure for Exposure B, at height = 30, I = 1 (Step 4)

Or use **Table 5** below to calculate Design Wind Load.

The Design Wind Load will be used in **Part II** to select the appropriate SOLARMOUNT Series rail, rail span and foot spacing.

In **Part II**, use both the positive (downforce) and the negative (uplift) results from this calculation.

Table 4. Adjustment Factor (λ) for Roof Height & Exposure Category

		Exposure	
Nean roof neight (ft)	В	С	D
15	1.00	1.21	1.47
20	1.00	1.29	1.55
25	1.00	1.35	1.61
30	1.00	1.40	1.66
35	1.05	1.45	1.70
40	1.09	1.49	1.74
45	1.12	1.53	1.78
50	1.16	1.56	1.81
55	1.19	1.59	1.84
60	1.22	1.62	1.87

Source: ASCE/SEI 7-05, Minimum Design Loads for Buildings and Other Structures, Chapter 6, Figure 6-3, p. 44.

Table 5. Worksheet for Components and Cladding Wind Load Calculation: IBC 2009, ASCE 7-05

Variable Description	Symbol	Value	Unit	Step	Reference
Building Height	h		ft		
Building, Least Horizontal Dimension			ft		
Roof Pitch			degrees		
Exposure Category				6	
Basic Wind Speed	V		mph		Figure I
Effective Wind Area			sf		
				2	
Roof Zone Setback Length	a		ft	3	Table I
Roof Zone Location				3	Figure 2
Net Design Wind Pressure	Pnet30		psf	4	Table 2, 3
Topographic Factor	K_{zt}	×		5	
Adjustment factor for height and exposure category	λ	×		7	Table 4
Importance Factor	I	×		8	Table 5
Total Design Wind Load	p_{net}		psf	9	

Table 6. Occupancy Category Importance Factor

Category	Category Desicription	Building Type Examples	Non-Hurricane Prone Regions and Hurricane Prone Regions with Basic Wind Speed, V = 85-100 mph, and Alaska	Hurricane Prone Re- gions with Basic Wind Speed,V > 100mph
ŧ	Buildings and other structures that represent a low hazard to human life in the event of failure, including, but limited to:	 Agricultural facilities Certain Temporary facilities Minor Storage facilities 	0.87	0.77
п	All buildings and other structures except those listed in Occupancy Categories I, III, and IV.		Ü	1
III	Buildings and other structures that represent a substantial hazard to human life in the event of a failure, including, but not limited to:	 Buildings where more than 300 people congregate Schools with a capacity more than 250 Day Cares with a capacity more than 150 Buildings for colleges with a capacity more than 500 Health Care facilities with a capacity more than 50 or more resident patients Jails and Detention Facilities Power Generating Stations Water and Sewage Treatment Facilities Telecommunication Centers Buildings that manufacture or house hazardous materials 	1.15	1.15 -
≥	Buildings and other structures designated as essential facilities, including, but not limited to:	 Hospitals and other health care facilities having surgery or emergency treatment Fire, rescue, ambulance and police stations Designated earthquake, hurricane, or other emergency shelters Designated emergency preparedness communication, and operation centers Power generating stations and other public utility facilities required in an emergency Ancillary structures required for operation of Occupancy Category IV structures Aviation control towers, air traffic control centers, and emergency aircraft hangars Water storage facilities and pump structures required to maintain water pressure for fire suppression Buildings and other structures having critical national defense functions 	1.15	1.15

Source: IBC 2009, Table 1604.5, Occupancy Category of Buildings and other structures, p. 281; ASCE/SEI 7-05, Minimum Design Loads for Buildings and Other Structures, Table 6-1, p. 77





[1.2.2.] Procedure to Calculate Total Design Wind per ASCE 7-10

See page 4 for ASCE 7-05 procedure.

Step 1. Determine risk category, See Table 6

Buildings and other structures shall be classified, based on the risk to human life, health and welfare associated with their damage or failure by nature of their occupancy or use. For the purpose of applying flood, wind, snow, ice, and earthquake provisions. See Table 7 on page 11.

Tab	Table 7: Risk Category of Buildings and Other Structures for Flood, Wind, Snow, Earthquake, and Ice Loads						
	Use or Occupancy of Buildings and Structures	Risk Category					
Build	lings and other structures that represent a low risk to human life in the event of failure.	I					
All bi	uildings and other structures except those listed in Risk Categories I, III, and IV	II					
	Buildings and other structures, the failure of which could pose a substantial risk to human life						
	Buildings and other structures, not included in Risk Category IV, with potential to cause a substantial economic impact and/or mass disruption of day-to-day civilian life in the event of failure.	III					
	Buildings and other structures, not included in Risk Category IV (including, but not limited to, facilities that manufacture, process, handle, store, use, or dispose of such substances as hazardous fuels, hazardous chemicals, hazardous waste, or explosives) containing toxic or explosive substances where their quantity exceeds a threshold quantity established by authority having jurisdiction and is sufficient to pose a threat to the public if released.	111					
	Buildings and other structures designated as essential facilities.						
	Buildings and other structures, the failure of which could pose a substantial hazard to the community.						
	Buildings and other structures (including, but not limited to, facilities that manufacture, process, handle, store, use, or dispose of such substances as hazardous fuels, hazardous chemicals, or hazardous chemicals or hazardous waste) containing sufficient quantities of highly toxic substances where the quantity exceeds a threshold quantity established by the authority having jurisdiction to be dangerous to the public if released and is sufficient to pose a threat to the public if released. ^a	IV					
	Buildings and other structures required to maintain the functionality of other Risk Category IV structures.						

^aBuildings and other structures containing toxic, highly toxic, or explosive substances shall be eligible for classification to a lower Risk Category if it can be demonstrated to the satisfaction of the authority having jurisdiction by a hazard assessment as described in Section 1.5.2 of ASCE 7-10 that a release of the substances is commensurate with the risk associated with that Risk Category.

Step 2. Determine the Basic Wind Speed, V (mph)

Determine the basic wind speed, V (mph) by consulting your local department or by locating your installation on the maps in Figures 26.5 1a through 1c, pages 12 - 17. Please note that the wind speeds are dependent on the Risk (Occupancy) category determined in Step 1.



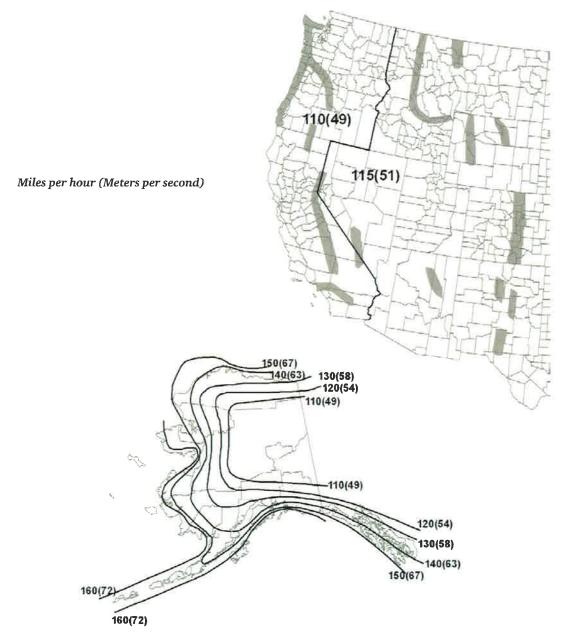


FIGURE 26.5-1A Basic Wind Speeds for Risk Category II Buildings and Other Structures

- 1. Values are design 3-second gust wind speeds in miles per hour (m/s) at 33 ft (10m) above ground for Exposure C category.
- 2. Linear interpolation between contours is permitted.
- 3. Islands and coastal areas outside the last contour shall use the last wind speed contour of the coastal area.
- 4. Mountainous terrain, gorges, ocean promontories, and special wind regions shall be examined for unusual wind conditions.
 5. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years).





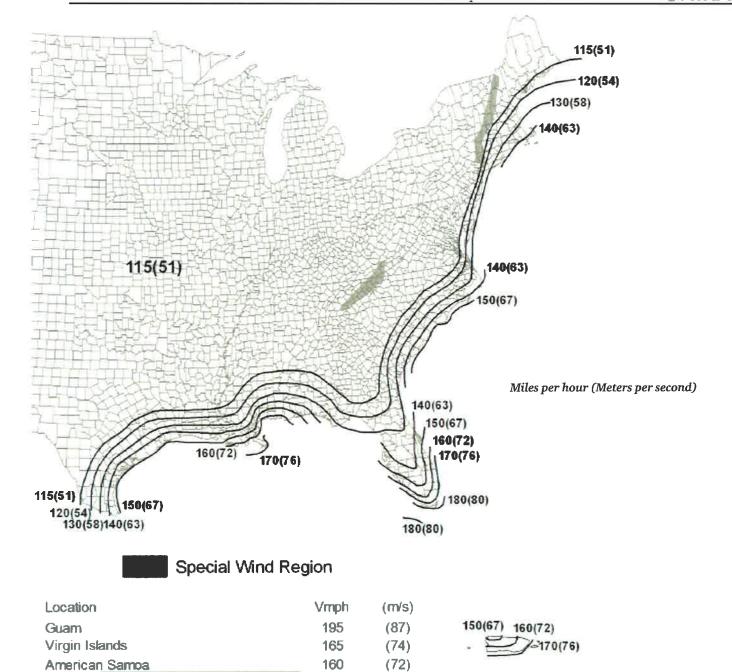


Figure 26.5-1A (Continued)

130

(58)



Puerto Rico

Source: ASCE 7-10 Minimum Design Loads for Buildings and Other Structures, Chapter 26

Hawaii - Special Wind Region Statewide

13

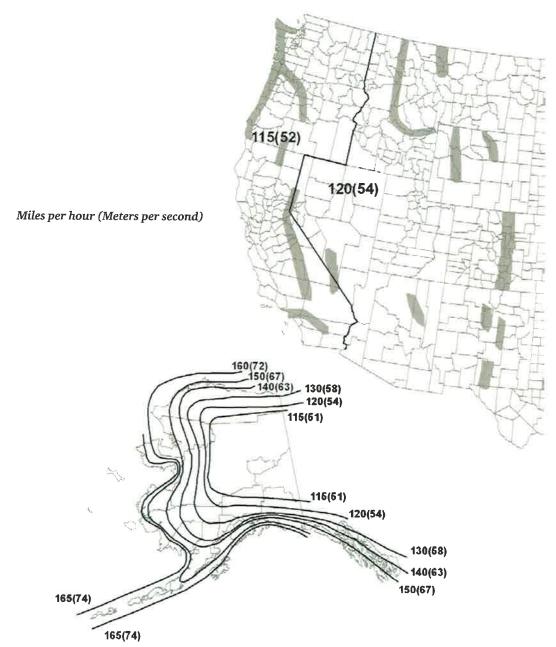


FIGURE 26.5-1B Basic Wind Speeds for Risk Category III and IV Buildings and Other Structures

Notes:

- 1. Values are design 3-second gust wind speeds in miles per hour (m/s) at 33 ft (10m) above ground for Exposure C category.
- 2. Linear interpolation between contours is permitted.
- 3. Islands and coastal areas outside the last contour shall use the last wind speed contour of the coastal area.
- 4. Mountainous terrain, gorges, ocean promontories, and special wind regions shall be examined for unusual wind conditions.
- 5. Wind speeds correspond to approximately a 3% probability of exceedance in 50 years (annual exceedance probability = 0.000588, MRI = 1700 years).

Source: ASCE 7-10 Minimum Design Loads for Buildings and Other Structures, Chapter 26

Compliance iniversal Engineering

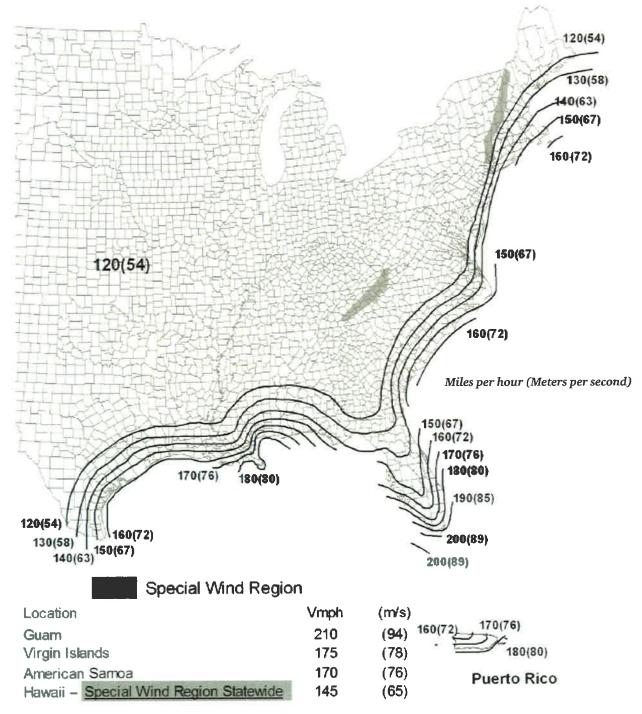


Figure 26.5-1B (Continued)



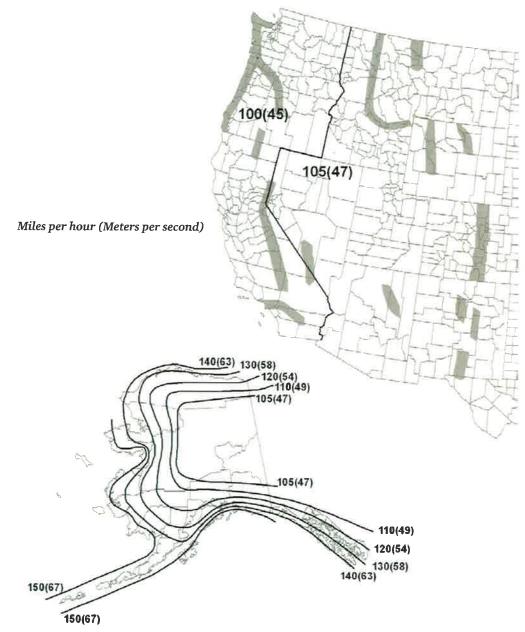


FIGURE 26.5-1C Basic Wind Speeds for Risk Category I Buildings and Other Structures

Notes:

- 1. Values are design 3-second gust wind speeds in miles per hour (m/s) at 33 ft (10m) above ground for Exposure C category.
- 2. Linear interpolation between contours is permitted.
- 3. Islands and coastal areas outside the last contour shall use the last wind speed contour of the coastal area.
- 4. Mountainous terrain, gorges, ocean promontories, and special wind regions shall be examined for unusual wind conditions.

 5. Wind speeds correspond to approximately a 15% probability of exceedance in 50 years (annual exceedance probability = 0.00333, MRI = 300 years).



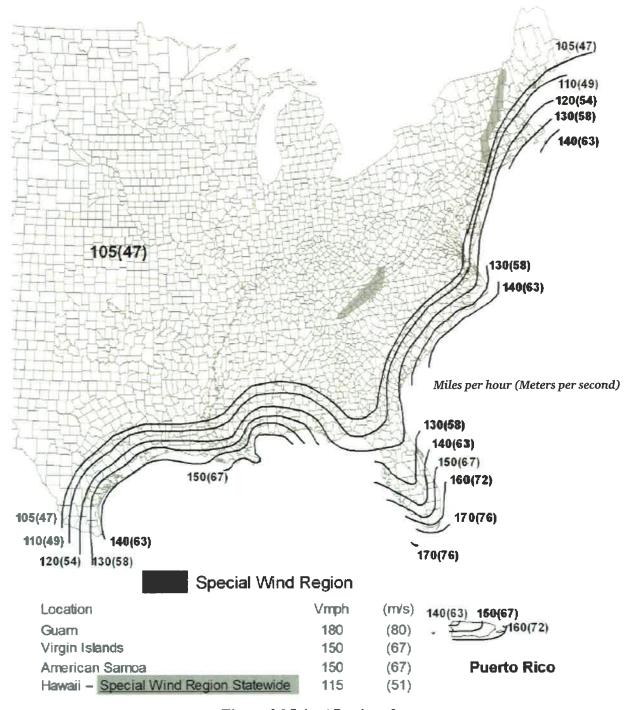


Figure 26.5-1c (Continued)



ASCE 7-10

Step 3. Determine Wind Load Parameters

Step 3a: Determine the proper Exposure Category (B, C, or D) for the project by using the following definitions for Surface Roughness Categories.

ASCE 7-10 defines wind surface roughness categories as follows:

Surface Roughness B: Urban and suburban areas, wooded areas, or other terrain with numerous closely spaced obstructions having the size of single-family dwellings or larger.

Surface Roughness C: Open terrain with scattered obstructions having heights generally less than 30 ft (9.1 m). This category includes flat open country and grasslands.

Surface Roughness D: Flat, unobstructed areas and water surfaces. This category includes smooth mud flats, salt flats, and unbroken ice.

Step 3b: Determine the Topographic Factor, K_{zt} . For the purposes of this code compliance document, the Topographic Factor, K_{zt} , is taken as equal to one (1) as per Section 26.8–2 or as determined by Figure 26.8–1 in ASCE 7–10.

Step 4. Determine Effective Wind Area
Determine the smallest area
of continuous modules you will be
installing. This is the smallest area
tributary (contributing load) to a support
or to a simple-span of rail. That area is
the Effective Wind Area, the total area of
the fewest number of modules on a run
of rails. If the smallest area of continuous
modules exceeds 100 sq ft, use 100 sq ft,
if less round down to values available in
Table 9, page 21.

Step 5. Determine the appropriate roof zone for the installation.

The Design Wind Load will vary based on where the installation is located on a roof. Arrays may be located in more than one roof zone.

Using Table 8, page 19, determine the Roof Zone Dimension Length, a (ft), according to the width and height of the building on which you are installing the pv system.



dimension or 3 ft of the building.

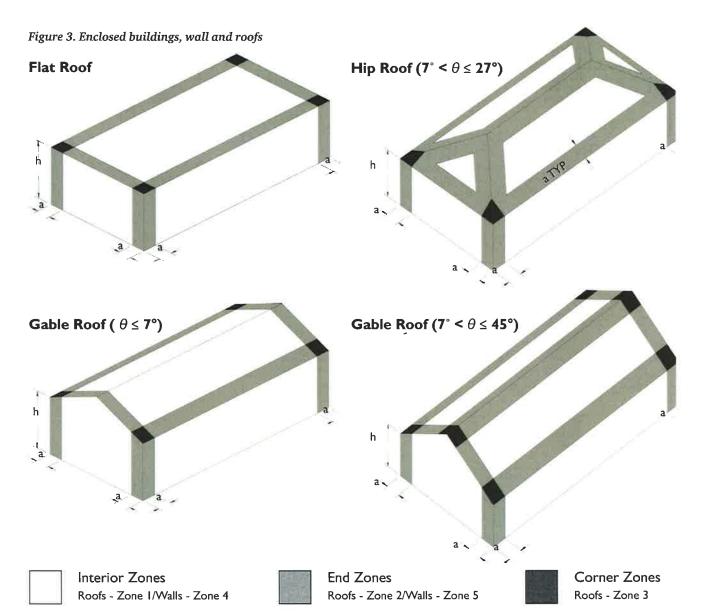


Table 8. Determine Roof/Wall Zone, dimension (a) according to building width and height a = 10 percent of the least horizontal dimension or 0.4h, whichever is smaller, but not less than either 4% of the least horizontal

Roof							Least	Horiz	ontal D	imensi	ion (ft)								
Height (ft)	10	15	20	25	30	40	50	60	70	80	90	100	125	150	175	200	300	400	500
10	3	3	3	3	3	4	4	4	.4	4	4	4	5	6	7	8	12	16	20
15	3	3	3	3	3	4	5	6	6	6	6	6	6	6	7	8	12	16	20
20	3	3	3	3	3	4	5	6	7	8	8	8	8	8	8	8	12	16	20
25	3	3	3	3	3	4	5	6	7	8	9	10	10	10	10	10	12	16	20
30	3	3	3	3	3	4	5	6	7	8	9	10	12	12	12	12	12	16	20
35	3	3	3	3	3	4	5	6	7	8	9	10	12.5	14	14	14	14	16	20
40	3	3	3	3	3	4	5	6	7	8	9	10	12.5	15	16	16	16	16	20
45	3	3	3	3	3	4	5	6	7	8	9	10	12.5	15	17.5	18	18	18	20
50	3	3	3	3	3	4	5	6	7	8	9	10	125	15	17.5	20	20	20	20
60	3	3	3	3	3	4	5	6	7	8	9	10	125	15	17.5	20	24	24	24

Step 5. Determine the appropriate roof zone for the installation (continued) Using the Roof Zone Dimension Length, a, determine the roof zone locations according to your roof type, gable, hip or monoslope. Determine in which roof zone your pv system is located, Zone 1, 2, or 3 according to Figure 3, page 20.





Source: ASCE/SEI 7-10, Minimum Design Loads for Buildings and Other Structures, Chapter 30, p. 345.

ASCE 7-10 Step 6. Determine Net Design Wind Pressure, p_{net30} (psf)

Using the Effective Wind Area (Step 4), Roof Zone Location (Step 5), and Basic Wind Speed (Step 2), look up the appropriate Net Design Wind Pressure in Table 9, page 21. Use the Effective Wind Area value in the table which is smaller than the value calculated in Step 2. If the installation is

located on a roof overhang, use Table 10, page 22. Both downforce and uplift pressures must be considered in overall design. Refer to Section II, Step 1 for applying downforce and uplift pressures. Positive values are acting toward the surface. Negative values are acting away from the surface.





	Components and Cladding – Method 1														h≤	60 ft				
Figu	ire 30	0.5-1 (c	ont'd)		Des	ign V	Vind	Press	ures		T								
	Encl	osed B	uildir	ıgs											Val.	ls &	: Ro	ofs		
			ı	Net D	esig	ın W	ind F	Pres	sure.	D _{not}	տ (p։	sf) <i>(E</i>	xposi	ıre B a	ath=	30 ft.)			
		Effective											eed V (mph)							
	Zone	wind area	_	10	4	45	4	20			_				- 44	~	- 4	20		
⊩	1	(8f) 10	_	_		15		20		30	_	40		50		60	_	80	_	00
	Ħ	20	8.9	-21.8 -21.2	9.7	-23.8 -23.2	10.5	-25.9 -25.2	12.4	-30.4 -29.6	14.3	-35.3 -34.4	16.5 15.4	-40.5 -39.4	18.7	-46.1 -44.9	23.7	-58.3 -56.8	29.3 27.4	-720 -70.1
•	1	50	7.6	-20.5	8.3	-22.4	9.0	-24.4	10.6	-28.6	12.3	-33.2	14.1	-38.1	16.0	43.3	20.3	-54.8	25.0	-67.7
8 9 8	1	100	7.0	-19.9	7.7	-21.8	8.3	-23.7	9.8	-27.8	11.4	-32.3	13.0	-37.0	14.8	421	18.8	-53.3	23.2	-65.9
	2	10	8.9	-36.5	9.7	-39.9	10.5	43.5	12.4	-51.0	14.3	-59.2	16.5	-67.9	18.7	<i>-</i> 77.3	23.7	-97.8	29.3	-120.7
2	2	20	8.3	-32.6	9.1	-35.7	9.9	-38.8	11.6	45.6	13.4	-52.9	15.4	-60.7	17.6	-69.0	22.2	-87.4	27.4	-107.9
ē	2	50	7.6	-27.5	8.3	-30.1	9.0	-32.7	10.6	-38.4	12.3	-44.5	14.1	-51.1	16.0	-58.2	20.3	-73.6	25.0	-90.9
Roof 0 to 7	2	100	7.0	-23.6	7.7	-25.8	8.3	-28.1	9.8	-33.0	11.4	-38.2	13.0	-43.9	14.8	-50.0	18.8	-63.2	23.2	-78.1
	3	10	8.9	-55.0	9.7	-60.1	10.5	-65.4	12.4	-76.8	14.3	-89.0	16.5	-1022	18.7	-116.3	23.7	-147.2	29.3	-181.7
	3	20 50	8.3 7.6	-45.5 -33.1	9.1 8.3	-49.8	9.9	-54.2 -39.3	11.6	-63.6	13.4	-73.8	15.4	-84.7	17.6	-96.3	22.2	-121.9	27.4	-150.5
11	3	100	7.0	-33.1	7.7	-36.1 -25.8	9.0	-38.3	10.6	-46.2 -33.0	12.3	-53.5 -38.2	14.1	-61.5 -43.9	16.0	-69.9 -50.0	20.3 18.8	-88.5 -63.2	25.0 23.2	-109.3 -78.1
⊩	1	10	12.5	-19.9	13.7	-21.8	14.9	-23.7	17.5	-27.8	20.3	-32.3	23.3	-37.0	28.5	421	33.6	-53.3	41.5	-65.9
Ш	$\pm i$	20	11.4	-19.4	12.5	-21.2	13.6	-23.0	16.0	-27.0	18.5	-31.4	21.3	-36.0	24.2	41.0	30.6	-51.9	37.8	-64.0
8	1	50	10.0	-18.6	10.9	-20.4	11.9	-22.2	13.9	-26.0	16.1	-30.2	18.5	-34.6	21,1	-39.4	26.7	49.9	329	-61.6
degreee	1	100	8.9	-18.1	9.7	-19.8	10.5	-21.5	12.4	-25.2	14.3	-29.3	16.5	-33.6	18.7	-38.2	23.7	48.4	29.3	-59.8
	2	10	12.5	-34.7	13.7	-37.9	14.9	41.3	17.5	-48.4	20.3	-56.2	23.3	-64.5	26.5	-73.4	33.6	-929	41.5	-114.6
10 27	2	20	11.4	-31.9	125	-34.9	13.6	-38.0	16.0	-44.6	18.5	-51.7	21.3	-59.3	24.2	-67.5	30.6	-85.4	37.8	-105.5
~	2	50	10.0	-28.2	10.9	-30.9	11.9	-33.6	13.9	-39.4	16.1	-45.7	18.5	-52.5	21.1	-59.7	26.7	-75.6	329	-93.3
Roof 3	2	100	8.9	-25.5	9.7	-27.8	10.5	-30.3	12.4	-35.6	14.3	-41.2	16.5	-47.3	18.7	-53.9	23.7	-68.2	29.3	-84.2
<u>&</u>	3	10	12.5	-51.3	13.7	-56.0	14.9	-61.0	17.5	<i>-</i> 71.6	20.3	-83.1	23.3	-95.4	26.5	-100.5	33.6	-137.3	41.5	-169.5
	3	20	11.4	-47.9	12.5	-52.4	13.6	-57.1	16.0	-67.0	18.5	-77.7	21.3	-89.2	24.2	-101.4	30.6	-128.4	37.8	-159.5
	3	50 100	10.0	-43.5 -40.2	10.9	-47.6 -44.0	11.9	-51.8 -47.9	13.9	-60.8 -56.2	16.1	-70.5 -65.1	18.5 16.5	-81.0 -74.8	21.1	-85.1	26.7 23.7	-116.6 -107.7	32.9 29.3	-143.9 -132.9
⊩	1	100	19.9	-21.8	21.8	-23.8	23.7	-25.9	27.8	30.4	32.3	-35.3	37.0	-/4.6 -40.5	42.1	46.1	53.3	-58.3	65.9	-720
	H	20	19.4	-20.7	21.2	-22.6	23.0	-24.6	27.0	-28.9	31.4	-33.5	36.0	-38.4	41.0	43.7	51.9	-55.3	64.0	-68.3
#	Hil	50	18.6	-19.2	20.4	-21.0	22.2	-22.8	26.0	-26.8	30.2	-31.1	34.6	-35.7	39.4	40.6	49.9	-51.4	61.6	-63.4
degrees	$\pm i$	100	18.1	-18.1	19.8	-19.8	21.5	-21.5	25.2	-25.2	29.3	-29.3	33.6	-33.6	38.2	-38.2	48.4	484	59.8	-59.8
1 8	2	100	19.9	-25.5	21.8	-27.8	23.7	-30.3	27.8	-35.6	32.3	-41.2	37.0	-47.3	42.1	-53.9	53.3	-88.2	65.9	-84.2
to 45	2	20	19.4	-24.3	21.2	-26.6	23.0	-29.0	27.0	34.0	31.4	-39.4	36.0	-45.3	41.0	-51.5	51.9	-65.2	64.0	-80.5
27 t	2	50	18.6	-22.9	20.4	-25.0	22.2	-27.2	26.0	-320	30.2	-37.1	34.6	-425	39.4	48.4	49.9	-61.3	61.6	-75.6
I A	2	100	18.1	-21.8	19.8	-23.8	21.5	-25.9	25.2	-30.4	29.3	-35.3	33.6	-40.5	38.2	-46.1	48.4	-58.3	59.8	-720
Roof	3	10	19.9	-25.5	21.8	-27.8	23.7	-30.3	27.8	-35.6	32.3	-41.2	37.0	-47.3	42.1	-53.9	53.3	-68.2	65.9	-84.2
	3	20	19.4	-24.3	21.2	-26.6	23.0	-29.0	27.0	-34.0	31.4	-39.4	36.0	-45.3	41.0	-51.5	51.9	-65.2	64.0	-80.5
	3	50	18.6	-22.9	20.4	-25.0	22.2	-27.2	26.0	-320	30.2	-37.1	34.6	-425	39.4	48.4	49.9	-61.3	61.6	-75.6
	3	100	18.1	-21.8	19.8	-23.8	21.5	-25.9	25.2	-30.4	29.3	-35.3	33.6	-40.5	38.2	-46.1	48.4	-58.3	59.8	-720
	4	10	21.8	-23.6	23.8	-25.8	25.9	-28.1	30.4	-33.0	35.3	-38.2	40.5	-43.9	46.1	-50.0	58.3	-63.2	72.0	-78.1
	4	20	20.8	-22.6	22.7	-24.7	24.7	-26.9	29.0	-31.6	33.7	-36.7	38.7	-421	44.0	-47.9 -45.1	55.7	-60.6	68.7	-74.8
	4	100	19.5	-21.3	21.3	-23.3	23.2	-25.4	27.2	-29.8	31.6	-34.6	36.2	-39.7	41.2	45.1	52.2	-57.1	64.4	-70.5
	4	100 500	18.5	-20.4 -18.1	20.2 17.7	-22.2 -19.8	22.0 19.3	-24.2 -21.5	25.9 22.7	-28.4 -25.2	30.0 26.3	-33.0 -29.3	34.4	-37.8 -33.6	39.2 34.3	-43.1 -38.2	49.6 43.5	-54.5 -48.4	61.2 53.7	-67.3 -59.8
Wa	5	10	21.8	-29.1	23.8	-31.9	25.9	-21.5	30.4	40.7	35.3	-29.3 -47.2	40.5	-54.2	46.1	-36.2 -61.7	58.3	-78.0	72.0	-96.3
	5	20	20.8	-27.2	22.7	-29.7	24.7	32.4	29.0	-38.0	33.7	-44.0	38.7	-50.5	44.0	-57.5	55.7	-728	68.7	-89.9
	5	50	19.5	-24.6	21.3	-28.9	23.2	-29.3	27.2	34.3	31.6	-39.8	36.2	45.7	41.2	-52.0	52.2	-65.8	64.4	-81.3
	5	100	18.5	-22.6	20.2	-24.7	22.0	-26.9	25.9	-31.6	30.0	-36.7	34.4	-421	39.2	47.9	49.6	-60.6	61.2	-74.8
	5	500	16.2	-18.1	17.7	-19.8	-	-21.5	22.7	-25.2	26.3	-29.3	30.2	-33.6	34.3	-38.2	43.5	48.4	53.7	-59.8
Note:	For eff	ective are		-				_												

Table 9. $p_{net_{30}}$ (psf) Roof and Wall

Note: For effective areas between the those given above the load may be interpolated, otherwise use the load associated with the lower effective area.



Roof Overhang Net Design Wind Pressure, p_{net30} (psf) (Exposure B at h = 30 ft.)

П		Effective		Ba	sic Wir	id Spee	d V (mp	oh)		
П		Wind Area								
	Zone	(54)	110	115	130	140	150	160	180	200
П	2	10	-31.4	-34.3	-43.8	-50.8	-58.3	-66.3	-84.0	-103.7
Ш	2	20	-30.8	-33.7	-43.0	-49.9	-57.3	-65.2	-82.5	-101.B
اءا	2	50	-30.1	-32.9	-42.0	-48.7	-55.9	-63.6	-80.5	-99.4
degreee	2	100	-29.5	-32.3	-41.2	-47.8	-54.9	-62.4	-79.0	-97.6
- P	3	10	-51.6	-56.5	-72.1	-83.7	-96.0	-109.3	-138.3	-170.7
Roof 0 to 7	3	20	-40.5	-44.3	-56.6	-65.7	-75.4	-85.8	-108.6	-134.0
۽ ا	3	50	-25.9	-28.3	-36.1	-41.9	-48.1	-54.7	-69.3	-85.5
ê	3	100	-14.8	-16.1	-20.6	-23.9	-27.4	-31.2	-39.5	-48.8
П	2	10	-40.6	-44.4	-56.7	-65.7	-75.5	-85.9	-108.7	-134.2
	2	20	-40.6	-44.4	-56.7	-65.7	-75.5	-85.9	-108.7	-134.2
	2	50	-40.6	-44.4	-56.7	-65.7	-75.5	-85.9	-108.7	-134.2
ee au Bep	2	100	-40.6	-44.4	-56.7	-65.7	-75.5	-85.9	-108.7	-134.2
2	3	10	-68.3	-74.6	-95.3	-110.6	-126.9	-144.4	-1828	-225.6
7 to	3	20	-61.6	-67.3	-86.0	-99.8	-114.5	-130.3	-164.9	-203.6
<u>^</u>	3	50	-52.8	-57.7	-73.7	-85.5	-98.1	-111.7	-141.3	-174.5
Roof	3	100	-46.1	-50.4	-64.4	-74.7	-85.8	-97.6	-123.5	-152.4
	2	10	-36.9	-40.3	-51.5	-59.8	-68.6	-78.1	-98.8	-122.0
ا ۽ ا	2	20	-35.8	-39.1	-50.0	-58.0	-66.5	<i>-</i> 75.7	-95.8	-118.3
degrees	2	50	-34.3	-37.5	-47.9	-55.6	-63.8	-72.6	-91.9	-113.4
8	2	100	-33.2	-36.3	-46.4	-53.8	-61.7	-70.2	-88.9	-109.8
54 65	3	10	-36.9	-40.3	-51.5	-59.8	-68.6	-78.1	-98.8	-122.0
27 to	3	20	-35.8	-39.1	-50.0	-58.0	-66.5	-75.7	-95.8	-118.3
Roof >	3	50	-34.3	-37.5	-47.9	-55.6	-63.8	-72.6	-91.9	-113.4
å	3	100	-33.2	-36.3	-46.4	-53.8	-61.7	-70.2	-88.9	-109.8

Table 10. p_{net30} (psf) Roof Overhang

Step 7. Determine adjustment factor for height and exposure category, I

Using the Exposure Category (Step 3) and the roof height, h (ft), look up the adjustment factor for height and exposure (λ) in Table 11, page 23.



		Exposure	
Mean roof height (ft)	В	С	D
15	1.00	1.21	1.47
20	1.00	1.29	1.55
25	1.00	1.35	1.61
30	1.00	.40	1.66
35	1.05	1.45	1.70
40	1.09	1.49	1.74
45	1.12	1.53	78
50	1.16	1.56	1.81
55	1.19	1.59	.84
60	1.22	.62	1.87

Step 8. Calculate the adjusted wind pressures, p_{net} , (psf)

Multiply the Net Design Wind Pressure, p_{net30} by the adjustment factor for height and exposure, I, the Topographic Factor, K_{zt} .

Where

I = adjustment factor for building height and exposure (Step 7)

 K_{zt} = For the purposes of this code compliance document, the Topographic Factor, K_{zt} , is taken as equal to one (1) as per Section 26.8-2 or as determined by Figure 26.8-1 in ASCE 7-10.

 $P_{\text{net}_{30}}$ = net design wind pressure for Exposure B, at h = 30 ft (Step 6)

The adjusted wind pressures will be used to select the appropriate SOLARMOUNT rail, rail span and attachment spacing.

Use both the positive (downforce) and the negative (uplift) results from this calculation.



Part II. Procedure to Select Rail Span and Rail Type

ASCE 7-05

[2.1.1.] Using Standard Beam Calculations, Structural Engineering Methodology ASCE 7-05

The procedure to determine the Unirac SOLARMOUNT series rail type and rail span uses standard beam calculations and structural engineering methodology. The beam calculations are based on a simply supported beam conservatively, ignoring the reductions allowed for supports of continuous beams over multiple supports. Please refer to **Part I** for more information on beam calculations, equations and assumptions. If beams are installed perpendicular to the eaves on a roof steeper than a 4/12 pitch in an area with a ground snow load greater than 30psf, then additional analysis is required for side loading on the roof attachment and beam.

In using this document, obtaining correct results is dependent upon the following:

- 1. Obtain the *Snow Load* for your area from your local building official.
- 2. Obtain the *Design Wind Load*, p_{net} . See Part I (Procedure to Determine the Design Wind Load) for more information on calculating the *Design Wind Load*.
- 3. *Please Note:* The terms rail span and footing spacing are interchangeable in this document. See **Figure 4** for illustrations
- 4. To use **Table 14** the *Dead Load* for your specific installation must be less than or equal to 5 psf, including modules and Unirac racking systems.

The following procedure will guide you in selecting a Unirac rail for a flush mount installation. It will also help determine the design loading imposed by the Unirac PV Mounting Assembly that the building structure must be capable of supporting.

Step 1: Determine the Total Design Load

The *Total Design Load*, *P* (*psf*) is determined using ASCE 7-05 2.4.1 (ASD Method equations 3,5,6 and 7) by adding the *Snow Load*¹, S (psf), *Design Wind Load*, *p*_{net} (*psf*) from Part I, Step 9, Page 9 and the *Dead Load* (*psf*). Both Uplift and Downforce Wind Loads calculated in Step 9 of Part 1, Page 9 must be investigated. Use Table 12, below, to calculate the Total Design Load for the load cases. Use the maximum absolute value of the three downforce cases and the uplift case for sizing the rail. Use the uplift case only for sizing lag bolts pull out capacities (Part II, Step 6). Use the following equations *or* Table 12, below.

 $P(psf) = 1.0D + 1.0S^1$ (downforce case 1)

 $P(psf) = 1.0D + 1.0p_{net}$ (downforce case 2)

 $P(psf) = 1.0D + 0.75S^{1} + 0.75p_{net}$ (downforce case 3)

 $P(psf) = 0.6D + 1.0p_{net} \text{ (uplift)}$

 $D = Dead \ Load \ (psf)$

 $S = Snow \ Load \ (psf)$

 p_{net} = Design Wind Load (psf) (Positive for downforce, negative for uplift)

The maximum Dead Load, D (psf), is 5 psf based on market research and internal data.

¹ Snow Load Reduction - The snow load can be reduced according to Chapter 7 of ASCE 7-05. The reduction is a function of the roof slope, Exposure Factor, Importance Factor and Thermal Factor. Please refer to Chapter 7 of ASCE 7-05 for more information.

Table 12. ASCE 7-05 Load Combinations

Description	Variable	Downforce Case 1	Downforce Case 2	Downforce Case 3	Uplift	units
Dead Load	D	1.0 ×	1.0 x	1.0 x	0.6 x	psf
Snow Load	S	1.0 x +		0.75 x +		psf
Design Wind Load Total Design Load	Pnet P		1.0 × +	0.75 x +	1.0 x -	psf psf

Note: Table to be filled out or attached for evaluation.





ASCE 7-10

[2.1.2.] Using Standard Beam Calculations, Structural Engineering Methodology ASCE 7-10

Step 1. Determine the Total Design Load

The Total Design Load, P (psf) is determined using ASCE 7-10 2.4.1 (ASD Method equations 3, 5, 6a and 7) by adding the Snow Load, S (psf), Design Wind Load, p_{net} (psf) from Step 8, Page 23 of section 1.2.2 and the Dead Load (psf). Both Uplift and Downforce Wind Loads calculated in Step 8, Page 23 of section 1.2.2 must be investigated. Use Table 13 to calculate the Total Design Load for the load cases. Use the maximum absolute value of the three downforce cases and the uplift case for sizing the rail. Use the uplift case only for sizing lag bolts pull out capacities. Use the following equations or Table 13, below.

 $P(psf) = 1.0D + 1.0S^1$ (downforce case 1)

 $P(psf) = 1.0D + 0.6p_{net}$ (downforce case 2)

 $P(psf) = 1.0D + 0.75S^{1} + 0.75(0.6p_{net})$ (downforce case 3)

 $P(psf) = 0.6D + 0.6p_{net} \text{ (uplift)}$

D = Dead Load (psf)

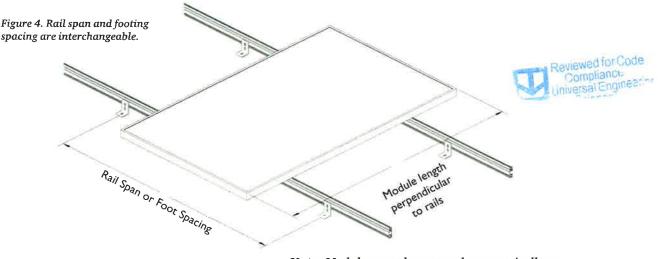
S = Snow Load (psf)

 p_{net} = Design Wind Load (psf) (Positive for downforce, negative for uplift)

Table 13. ASCE 7-10 Load Combinations

Description	Variable	Downforce Case I	Downforce Case 2	Downforce Case 3	Uplift	units
Dead Load	D	1.0 x	1.0 x	1.0 x	0.6 ×	psf
Snow Load	S	1.0 x +		0.75 x +		psf
Design Wind Load Total Design Load	Pnet P		0.6 × +	0.75 x +	0.6 × -	psf psf

Note: Table to be filled out or attached for evaluation.



Note: Modules must be centered symmetrically on the rails $(+/-2^*)$, as shown.

ASCE 7-05 AND ASCE 7-10

Step 2: Determine the Distributed Load on the rail, w (plf)

Determine the *Distributed Load*, *w* (*plf*), by multiplying the module length, B (ft), by the *Total Design Load*, *P* (*psf*) and dividing by two. Use the maximum absolute value of the three downforce cases and the Uplift Case. We assume each module is supported by two rails.

w = PB/2

 $w = Distributed\ Load\ (pounds\ per\ linear\ foot,\ plf)$

B = Module Length Perpendicular to Rails (ft)

P = Total Design Pressure (pounds per square foot, psf)

Step 3: Determine Rail Span/L-Foot Spacing

Using the *distributed load*, *w*, from Part II, **Step 2**, look up the *allowable spans*, *L*, for each Unirac rail type, SOLARMOUNT (SM) and SOLARMOUNT Heavy Duty (HD) in table 14.

The L-Foot SOLARMOUNT Series Rail Span Table uses a single L-foot connection to the roof, wall or stand-off. Please refer to the **Part III** for more installation information.

Table 14. L-Foot SOLARMOUNT Series Rail Span SM - SOLARMOUNT HD - SOLARMOUNT Heavy Duty

Span							Distrib	buted Load (pounds/line	ar foot)						
(ft)	20	25	30	40	50	60	80	100	120	140	160	180	200	220	240	260
2	SM	SM	SM	SM	SM	SM	SM	SM	SM	SM						
2.5	SM	SM	SM	SM	SM	SM	SM	HD	HD	HD						
3	SM	SM	SM	SM	SM	HD	HD	HD	HD	HD						
3.5	SM	SM	SM	SM	HD	HD	HD	HD	1123							
4	SM	SM	SM	HD	HD	HD	HD									
4.5	SM	SM	HD	HD	HD											
5	SM	SM	HD	HD	HD											
5.5	SM	HD	HD	HD												
6	SM	HD	HD													
6.5	SM	HD	HD													
7	SM	SM	SM	SM	SM	SM	HD	HD								
7.5	SM	SM	SM	SM	SM	SM	HD	HD								
8	SM	SM	SM	SM	SM	SM	HD	HD								
8.5	SM	SM	SM	SM	SM	HD	HD									
9	SM	SM	SM	SM	HD	HD	HD									
9.5	SM	SM	SM	SM	HD	HD	HD									
10	SM	SM	SM	HD	HD	HD	HD									
10.5	SM	SM	SM	HD	HD	HD										
ш	SM	SM	HD	HD	HD	HD										
11.5	SM	HD	HD	HD	HD	HD										
12	SM	HD	HD	HD	HD	HD										





Step 4: Select Rail Type

Selecting a span and rail type affects the price of your installation. Longer spans produce fewer wall or roof penetrations. However, longer spans create higher point load forces on the building structure. A point load force is the amount of force transferred to the building structure at each connection.

It is the installer's responsibility to verify that the building structure is strong enough to support the point load forces.

Step 5: Determine the Downforce Point Load, R (lbs), at each connection based on rail span

When designing the Unirac Flush Mount Installation, you must consider the downforce Point Load, R (lbs) on the roof structure.

The Downforce, Point Load, R (lbs), is determined by multiplying the Total Design Load, P(psf) (Step 1) by the Rail Span, L(ft) (Step 3) and the Module Length Perpendicular to the Rails, B (ft) divided by two.

R(lbs) = PLB/2

R = Point Load (lbs)

P = Total Design Load (psf)

L = Rail Span (ft)

B = Module Length Perpendicular to Rails (ft)

It is the installer's responsibility to verify that the building structure is strong enough to support the maximum point loads calculated according to Step 5.

Table 15. Downforce Point Load Calculation

Total Design Load (downforce) (max of case 1, 2 or 3):	Р		psf	Step 1
Module length perpendicular to rails:	В	X	ft	
Rail Span:	L	<u>×</u>	ft	Step 4
		/2		
Downforce Point Load:	R		lbs	



Step 6: Determine the Uplift Point Load, R (lbs), at each connection based on rail span

You must also consider the Uplift Point Load, R (lbs), to determine the required lag bolt attachment to the roof (building) structure.

Table 16. Uplift Point Load Calculation

Total Design Load (uplift):	Р		psf	Step I	
Module length perpendicular to rails:	В	×	ft	•	
Rail Span:	L	×	ft	Step 4	
			/2		
Uplift Point Load:	R		lbs		

Table 17. Lag pull-out (withdrawal) capacities (lbs) in typical roof lumber (ASD)

		Lag screw specifications	
	Specific	5/16" shaft,*	-
	gravity	per inch thread depth	
Douglas Fir, Larch	0.50	266	an an
Douglas Fir, South	0.46	235	
Engelmann Spruce, Lodgepole Pine (MSR 1650 f & higher)	0.46	235	
Hem, Fir, Redwood (close grain)	0.43	212	!
Hem, Fir (North)	0.46	235	Î
Southern Pine	0.55	307	Thread depth
Spruce, Pine, Fir	0.42	205	İ
Spruce, Pine, Fir (E of 2 million psi and higher			Y :
grades of MSR and MEL)	0.50	266	

Sources: American Wood Council, NDS 2005, Table 11.2A, 11.3.2A.

Notes: (1) Thread must be embedded in the side grain of a rafter or other structural member integral with the building structure.

- (2) Lag bolts must be located in the middle third of the structural member.
- (3) These values are not valid for wet service.
- (4) This table does not include shear capacities. If necessary, contact a local engineer to specify lag bolt size with regard to shear forces.
- (5) Install lag bolts with head and washer flush to surface (no gap). Do not over-torque.
- (6) Withdrawal design values for lag screw connections shall be multiplied by applicable adjustment factors if necessary. See Table 10.3.1 in the American Wood Council NDS for Wood Construction.

Use **Table 12** to select a lag bolt size and embedment depth to satisfy your Uplift Point Load Force, R (lbs), requirements. Divide the uplift pointload (from **Table 11**) by the withdrawal capacity in the 2nd column of **Table 12**. This results in inches of 5/16 lagbolt embedded thread depth needed to counteract the uplift force. If other than lag bolt is used (as with a concrete or steel), consult fastener mfr documentation.

It is the installer's responsibility to verify that the substructure and attachment method is strong enough to support the maximum point loads calculated according to Step 5 and Step 6.



^{*}Use flat washers with lag screws.



Part III. Installing SOLARMOUNT

The Unirac Code-Compliant Installation Instructions support applications for building permits for photovoltaic arrays using Unirac PV module mounting systems.

This manual, SOLARMOUNT Planning and Assembly, governs installations using the SOLARMOUNT and SOLARMOUNT HD (Heavy Duty) systems.

[3.1.] SOLARMOUNT rail components





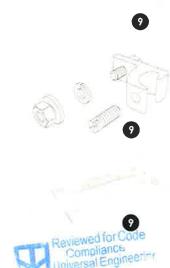


Figure 5. SOLARMOUNT rail components

- Rail Supports PV modules. Use two per row of modules. Aluminum extrusion, available in mill finish, clear anodized, or dark anodized.
- 2 Rail splice Joins and aligns rail sections into single length of rail. It can form either a rigid or thermal expansion joint, 8 inches long, predrilled. Aluminum extrusion, anodized, clear or dark.
- 3 Self-drilling screw (No. 10 x ¾") Use 4 per rigid splice or 2 per expansion joint. Galvanized steel. Supplied with splice.
- 4 L-foot Use to secure rails either through roofing material to building structure or standoffs. Refer to loading tables or U-Builder for spacing.
- **5** L-foot bolt (3/8" x ¾") Use one per L-foot to secure rail to L-foot. Stainless steel. Supplied with L-foot.
- Flange nut (3/8") Use one per L-foot to secure rail to L-foot. Stainless steel. Supplied with L-foot

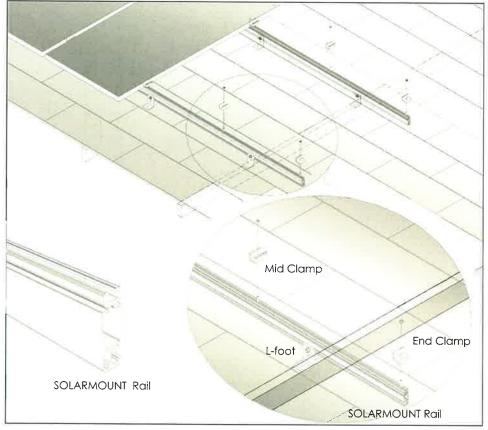
- Aluminum two-piece standoff (optional) (3", 4", 6" or 7" total height) – Use one per L-foot. Includes 3/8" x 3/4" serrated flange bolt with EPDM washer for attaching L-foot. Unirac offers flashings for use with
- 8 Top Mounting Clamps Includes T-bolts.
- Top Mounting Grounding Clips and Lugs

Installer supplied materials:

- Lag screw for L-foot Attaches L-foot or standoff to rafter. Determine the length and diameter based on pullout values. If lag screw head is exposed to elements, use stainless steel. Under flashings, zinc plated hardware is adequate.
- Waterproof roofing sealant Use a sealant appropriate to your roofing material. Consult with the company currently providing warranty of roofing.

[3.2.] Installing SOLARMOUNT & SMHD with top mounting clamps

This section covers SOLARMOUNT standard and SMHD rack assembly where the installer has elected to use top mounting clamps to secure modules to the rails. It details the procedure for flush mounting SOLARMOUNT systems to a pitched roof.



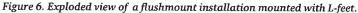




Table	18.	Wrenches	and	Torque
-------	-----	----------	-----	--------

	Wrench size	* Recommended torque (ft-lbs)
¼" hardware	7/16"	10 🛆
3/8" hardware	9/16"	30

Torques are not designated for use with wood connectors



All top down clamps must be installed with anti-seize lubricant to prevent galling and provide uniformity in clamp load. 1/4"-20 hardware used in conjunction with top down clamps must be installed to 10 ft-lbs of torque. When using UGC-1, UGC-2, WEEB 9.5 and WEEB 6.7, 1/4"-20 hardware must be installed to 10 ft-lbs of torque. Additionally, when used with a top down clamp, the module frame cross section must be boxed shaped as opposed to a single, l-shaped member. Please refer to installation supplement 910: Galling and Its Prevention for more information on galling and anti-seize and installation manual 225.6: Top Mounting Unirac Grounding Clips and WEEBLugs for more information on Grounding Clips.

^{*}With anti-seize



[3.2.1] Planning your SOLARMOUNT installations

The installation can be laid out with rails parallel to the rafters or perpendicular to the rafters. Note that SOLARMOUNT rails make excellent straight edges for doing layouts.

Center the installation area over the structural members as much as possible.

Leave enough room to safely move around the array during installation. Some building codes and fire codes require minimum clearances around such installations, and the user should be directed to also check 'The Code'.

The length of the installation area is equal to:

- the total width of the modules,
- plus 1 inch for each space between modules (for midclamp),
- plus 3 inches (1½ inches for each pair of end clamps).

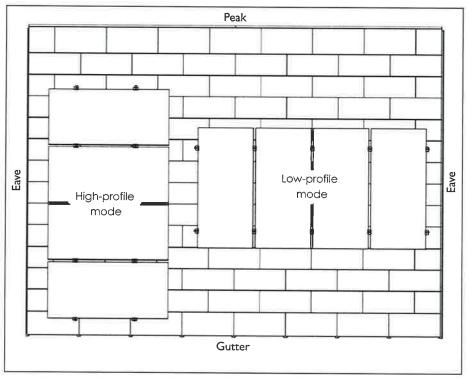


Figure 7. Rails may be placed parallel or perpendicular to rafters.



[3.2.2] Laying out L-feet for top clamps

L-feet (**Fig. 8**), in conjunction with proper flashing equipment and techniques, can be used for attachment through existing roofing material, such as asphalt shingles, sheathing or sheet metal to the building structure.

Use **Figure 9** below to locate and mark the position of the L-feet lag screw holes within the installation area.

If multiple rows are to be installed adjacent to one another, it is not likely that each row will be centered above the rafters. Adjust as needed, following the guidelines in **Figure 9** as closely as possible.



Figure 8

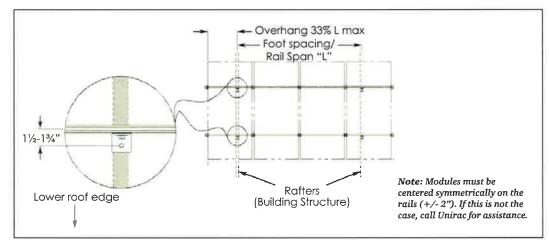


Figure 9. Layout with rails perpendicular to rafters.





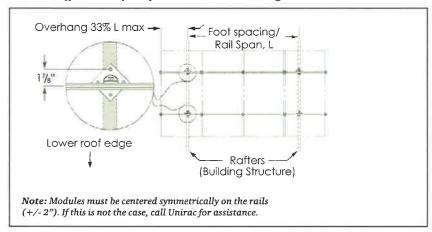
[3.2.3] Laying out standoffs

Standoffs (Figure 10) are used to increase the height of the array above the surface of the roof. Pair each standoff with a flashing to seal the lag bolt penetrations to the roof.

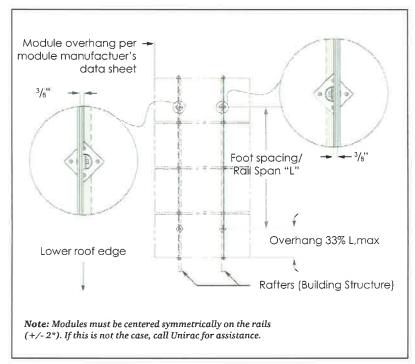
Use **Figure 11 or 12** to locate and mark the location of the standoff lag screw holes within the installation area.

Remove the tile or shake, if necessary, underneath each standoff location, exposing the roofing underlayment. Ensure that the standoff base lies flat on the underlayment, but remove no more material than required for the flashings to be installed properly.

The standoffs must be firmly attached to the building structure.



 $Figure\ 11.\ Layout\ with\ rails\ perpendicular\ to\ rafters. perpendicular\ to\ rafters.$



 $Figure\ 12.\ Layout\ with\ rails\ parallel\ to\ rafters.$



Figure 10. Standoff used in conjunction with an L-foot.

If multiple high-profile rows are to be installed adjacent to each other, it may not be possible for each row to be centered above the rafters. Adjust as needed, following the guidelines of Fig. 12 as closely as possible.

Installing standoffs:

Drill 3/16 inch pilot holes through the underlayment into the center of the rafters at each standoff location. Securely fasten each standoff to the rafters with the two 5/16" lag screws.

Ensure that the standoffs face as shown in Figure 11 or 12.

Unirac standoffs (1-5/8" O.D.) are designed for collared flashings available from Unirac.

Install and seal flashings and standoffs using standard building practices or as the company providing roofing warranty directs.



[3.2.4] Installing SOLARMOUNT rails

Keep rail slots free of roofing grit or other debris. Foreign matter will cause bolts to bind as they slide in the slots.

Installing Splices: If your installation uses SOLARMOUNT splice bars, attach the rails together (**Fig. 13**) before mounting the rails to the footings. Use splice bars only with flush installations or those that use low-profile tilt legs.

Although structural, the joint is not as strong as the rail itself. A rail should always be supported by *more than one* footing on *both* sides of the splice. (Reference installation manual 908, Splices/Expansion Joints.)

Mounting Rails on Footings: Rails may be attached to either of two mounting holes in the L-feet (**Fig. 14**). Mount in the lower hole for a low profile, more aesthetically pleasing installation. Mount in the upper hole for a higher profile, which will maximize airflow under the modules. This will cool them more and may enhance performance in hotter climates.

Slide the ¾-inch mounting bolts into the footing bolt slots. Loosely attach the rails to the footings with the flange nuts.

Aligning the Rail End: Align one pair of rail ends to the edge of the installation area (Fig. 15 or Fig. 16).

The opposite pair of rail ends will overhang the side of the installation area. Do not trim them off until the installation is complete.

If the rails are perpendicular to the rafters (Fig. 15), either end of the rails can be aligned, but the first module must be installed at the aligned end.

If the rails are parallel to the rafters (Fig. 16), the aligned end of the rails must face the lower edge of the roof. Securely tighten all hardware after alignment is complete (20 ft lbs).

Mount modules to the rails as soon as possible. Large temperature changes may bow the rails within a few hours if module placement is delayed.

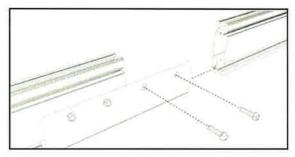


Figure 13. Splice bars slide into the footing bolt slots of SOLARMOUNT rail sections.

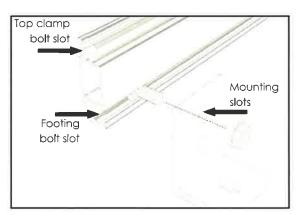


Figure 14. Foot-to-rail attachment



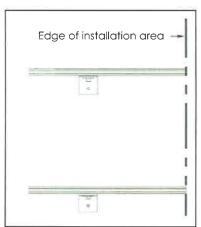
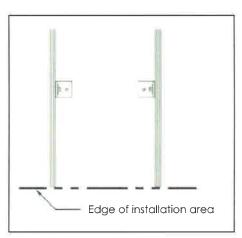


Figure 15. Rails perpendicular to the rafters.



Figure~16.~Rails~parallel~to~the~rafters.



[3.2.5] Installing the modules

Installing the First Module: In high-profile installations, the best practice would be to install a safety bolt ($\frac{1}{4}$ "-20 x $\frac{1}{2}$ ") and flange nut (both installer provided) fastened to the module bolt slot at the aligned (lower) end of each rail. It will prevent the lower end clamps and clamping bolts from sliding out of the rail slot during installation.

If there is a return cable to the inverter, connect it to the first module. Secure the first module with T-bolts and end clamps at the aligned end of each rail. Allow half an inch between the rail ends and the end clamps (**Fig.18**). Finger tighten flange nuts, center and align the module as needed, and securely tighten the flange nuts (10 ft lbs).

Installing the Other Modules: Lay the second module face down (glass to glass) on the first module. Connect intermodule cable to the second module. Turn the second module face up (Fig. 17). With T-bolts, mid-clamps and flange nuts, secure the adjacent sides of the first and second modules. Align the second module and securely tighten the flange nuts (Fig. 19).

For a neat installation, fasten wire management devices to rails with self-drilling screws.

Repeat the procedure until all modules are installed. Attach the outside edge of the last module to the rail with end clamps.

Trim off any excess rail, being careful not to cut into the roof. Allow half an inch between the end clamp and the end of the rail (Fig. 18).

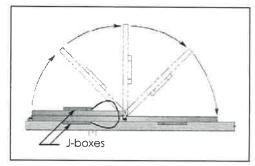


Figure 17

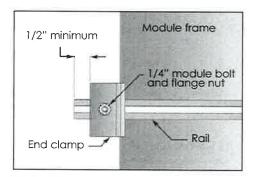


Figure 18

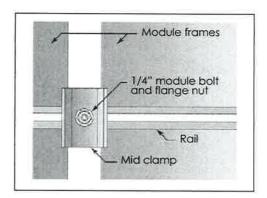


Figure 19



[3.3] Installing SOLARMOUNT with bottom mounting clips, HD rail only

This section covers SOLARMOUNT rack assembly where the installer has elected to use bottom mounting clamps to secure modules to the rails. It details the procedure for flush mounting SOLARMOUNT HD systems to a pitched roof.

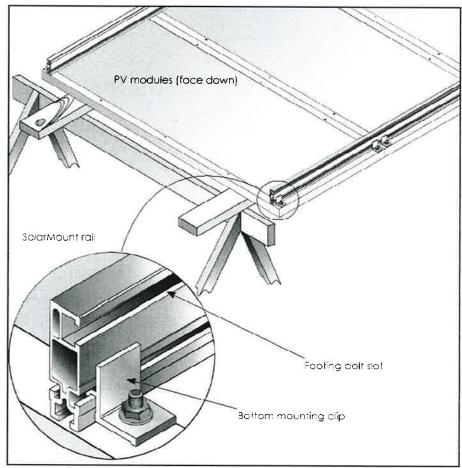


Figure 20. Installing bottom clips



Table 19. Wrenches and torque

Wrench size	* Recommended torque (ft-lbs)
7/16"	10
	size

Note: Torque specifications do not apply to lag bolt connections.



Stainless steel hardware can seize up, a process called galling. To significantly reduce its likelihood, (1) apply lubricant to bolts, preferably an anti-seize lubricant, available at auto parts stores, (2) shade hardware prior to installation, and (3) avoid spinning on nuts at high speed. See Installation Supplement 910, Galling and Its Prevention, at www.unirac.com.

^{*}With anti-seize

[3.3.1] Planning the installation area

Decide on an arrangement for clips, rails, and L-feet (Fig. 21).

Use Arrangement A if the full width of the rails contacts the module. Otherwise use Arrangement B.

Caution: If you choose Arrangement B, either (1) use the upper mounting holes of the L-feet or (2) be certain that the L-feet and clip positions don't

If rails must be parallel to the rafters, it is unlikely that they can be spaced to match rafters. In that case, add structural supports – either sleepers over the roof or mounting blocks beneath it. These additional members must meet code; if in doubt, consult a professional engineer.

Never secure the footings to the roof decking alone. Such an arrangement will not meet code and leaves the installation and the roof itself vulnerable to severe damage from wind.

Leave enough room to safely move around the array during installation. The width of a rail-module assembly equals the length of one module. Note that L-feet may extend beyond the width of the assembly by as much as 2 inches on each side. The length of the assembly equals the total width of the modules.

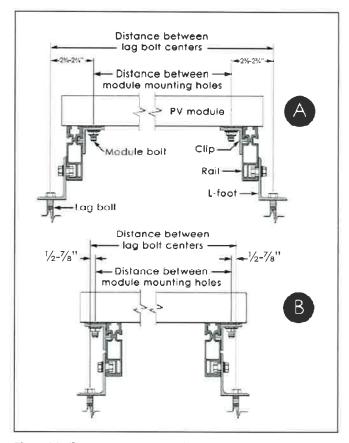


Figure 21. Clip Arrangements A and B



[3.3.2] Laying out the installing L-feet for bottom clips

L-feet, in conjunction with proper flashing equipment and techniques, are used for installation through existing low profile roofing material, such as asphalt shingles or sheet metal. They are also used for most ground mount installations. To ensure that the L-feet will be easily accessible during flush installation:

- Use the PV module mounting holes nearest the ends of the modules.
- Situate the rails so that footing bolt slots face outward.

The single slotted side of the L-foot must always lie against the roof with the double-slotted side perpendicular to the roof.

Foot spacing (along the same rail) and rail overhang depend on design wind loads.

Install half the L-feet:

- If rails are perpendicular to rafters (Fig. 22), install the feet closest to the lower edge of the roof.
- If rails are parallel to rafters
 (Fig. 23), install the feet for one of
 the rails, but not both.

Ensure that the L-feet face as shown in Figure 22 or Figure 23.

Hold the rest of the L-feet and fasteners aside until the panels are ready for the installation.

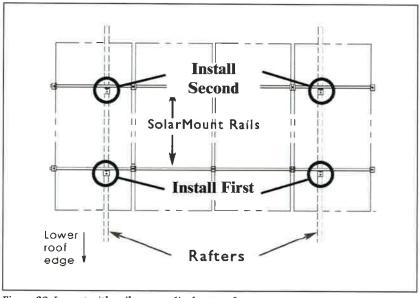


Figure 22. Layout with rails perpendicular to rafters.

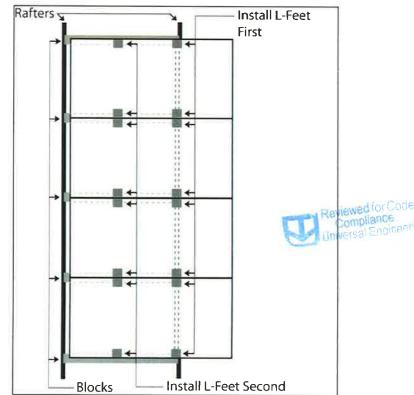


Figure 23. Layout with rails parallel to rafters.



[3.3.3] Attaching modules to the rails

Lay the modules for a given panel face down on a surface that will not damage the module glass. Align the edges of the modules and snug them together (Fig. 21, page 22).

Trim the rails to the total width of the modules to be mounted. Place a rail adjacent to the outer mounting holes. Orient the footing bolt slot outward. Place a clip slot adjacent to the mounting holes, following the arrangement you selected earlier.

Assemble the clips, mounting bolts, and flange nuts. Torque the flange nuts to 10 foot-pounds.

[3.3.4] Installing the module-rail assembly

Bring the module-rail assembly to the installation site. Keep rail slots free of debris that might cause bolts to bind in the slots.

Consider the weight of a fully assembled panel. Unirac recommends safety lines whenever lifting one to a roof.

Align the panel with the previously installed L-feet. Slide 3/8 inch L-foot mounting bolts onto the rail and align them with the L-feet mounting holes. Attach the panel to the L-feet and finger tighten the flange nuts.

Rails may be attached to either of two mounting holes in the footings (Fig. 24).

- Mount in the lower hole for a low, more aethetically pleasing installation.
- Or mount in the upper hole to maximize a cooling airflow under the modules. This may enhance performance in hotter climates.

Adjust the position of the panel as needed to fit the installation area. Slide the remaining L-feet bolts onto the other rail, attach L-feet, and finger tighten with flange nuts. Align L-feet with mounting holes previously drilled into the roof. Install lag bolts into remaining L-feet as described in "Laying out and installing L-feet" above.

Torque all footing flange nuts to 30 foot-pounds. Verify that all lag bolts are securely fastened.

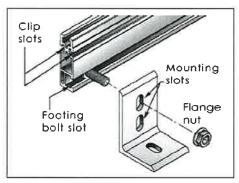


Figure 24. Leg-to-rail attachment



[3.4] Installing SOLARMOUNT with grounding clips and lugs

Clips and lugs are sold separately:



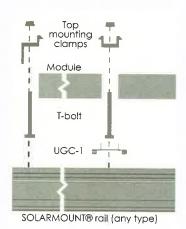


Figure 25. Slide UGC-1 grounding clip into top mounting slot of rail. Torque modules in place on top of clip. Nibs will penetrate rail anodization and create grounding path through rail.



Figure 26. Insert a bolt in the aluminum rail or through the clearance hole in the stainless steel flat washer. Place the stainless steel flat washer on the bolt, oriented so the dimples will contact the aluminum rail. Place the lug portion on the bolt and stainless steel flat washer. Install stainless steel flat washer, lock washer and nut. Tighten the nut until the dimples are completely embedded into the rail and lug. The embedded dimples make a gas-tight mechanical connection and ensure good electrical connection between the aluminum rail and the lug through the WEEB.

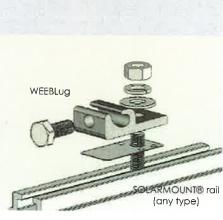
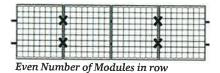
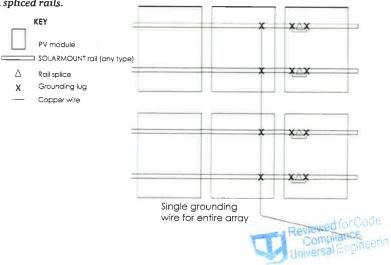


Figure 27. UGC-1 layout for even and odd number of modules in row. "X" denotes places to install UGC-1.



Odd Number of Modules in row

Figure 28. Single wire grounding with spliced rails.



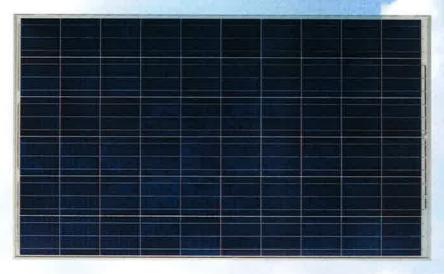


Worldwide Energy and Manufacturing USA Co., Limited

AS-6P30

Designed for maximum power output, AS-6P30 modules, offer higher power output over a longer period of time, 30-year warranty.





Special Warranties

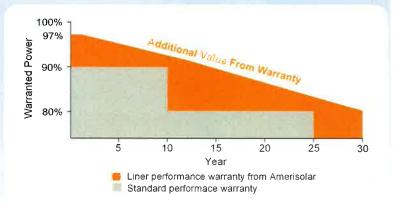
- 12 year limited product warranty.
- Limited power warranty: 12 years 91.2% of the nominal power output, 30 years 80.6% of the nominal power output.

Key Features

- High module conversion efficiency up to 16.29% through superior * manufacturing technology.
- Low degradation and excellent performance under high temperature and low * light conditions.
- Robust aluminum frame ensures the modules to withstand wind loads up to * 2400Pa and snow loads up to 5400Pa.
- Positive power tolerance of 0 ~ +3 %.
- High ammonia and salt mist resistance.

Quality Certificates

- IEC61215, IEC61730, IEC62716, IEC61701, UL1703, CE, MCS, CEC, Israel Electric, Kemco
- ISO9001:2008: Quality management system
- ISO14001:2004: Environmental management system
- OHSAS18001:2007: Occupational health and safety management system



















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Electrical Characteristics

Electrical parameters at STC								
Nominal Power (P _{max})	235W	240W	245W	250W	255W	260W	265W	
Open Circuit Voltage (Voc)	37.5V	37.7V	37.9V	38.0V	38.1V	38.2V	38.3V	
Short Circuit Current (I _{SC})	8.48A	8.57A	8.66A	8.75A	8.83A	8.90A	8.98A	
Voltage at Nominal Power (V _{mp})	29.7V	29.9V	30.1V	30.3V	30.5V	30.7V	30.9V	
Current at Nominal Power (I _{mp})	7.92A	8.03A	8.14A	8.26A	8.37A	8.47A	8.58A	
Module Efficiency (%)	14.44	14.75	15.06	15.37	15.67	15.98	16.29	

STC: Irradiance 1000W/m², Cell temperature 25°C, AM1.5

Electrical parameters at NOCT								
Nominal Power (P _{max})	172W	175W	179W	183W	186W	190W	194W	
Open Circuit Voltage (Voc)	34.5V	34.7V	34.9V	35.0V	35.1V	35.2V	35.3V	
Short Circuit Current (I _{SC})	6.87A	6.94A	7.01A	7.09A	7.15A	7.21A	7.27A	
Voltage at Nominal Power (V _{mp})	27.0V	27.2V	27.4V	27.6V	27.8V	27.9V	28.1V	
Current at Nominal Power (Imp)	6.38A	6.44A	6.54A	6.64A	6.70A	6.81A	6.91A	

NOCT: Irradiance 800W/m², Ambient temperature 20°C, Wind speed 1 m/s

Mechanical Characteristics

Cell type	Polycrystalline 156x156mm
Number of cells	60 (6x10)
Module dimension	1640x992x40mm
Weight	18.5kg
Front cover	3.2mm low-iron tempered glass
Frame	Anodized aluminum alloy
Junction box	IP67, 6 diodes
Cable	4mm², 900mm
Connector	MC4 or MC4 compatible
Standard packaging	26pcs/pallet
Module quantity per container	728pcs/40'HQ

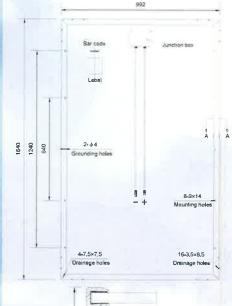
Temperature Characteristics

Nominal Operating Cell Temperature (NOCT)	45°C±2°C
Temperature Coefficients of P _{max}	-0.43%/°C
Temperature Coefficients of Voc	-0.33%/°C
Temperature Coefficients of I _{SC}	0.056%/°C

Maximum Ratings

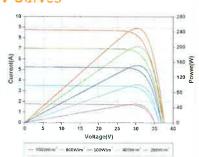
Operating Temperature	-40°C to +85°C
Maximum System Voltage	1000V DC
Maximum Series Fuse Rating	15A

Drawings

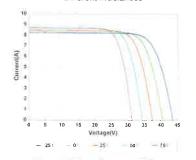




I-V Curves



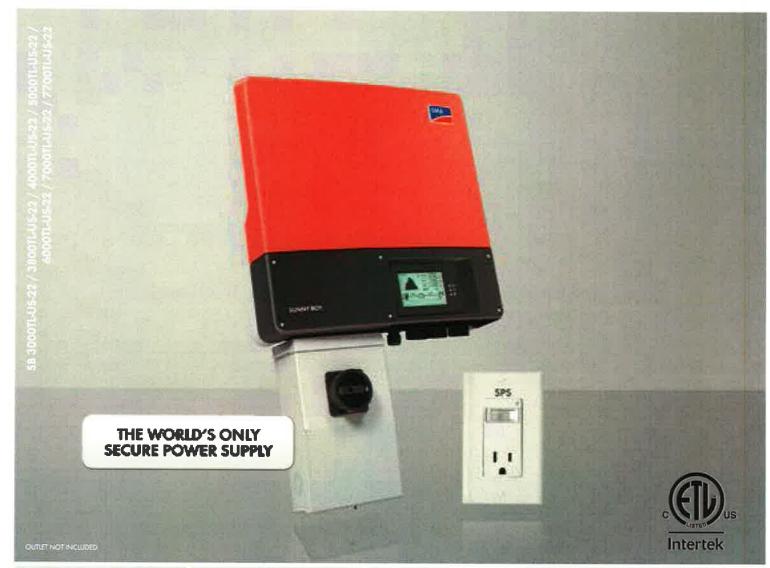
Current-Voltage and Power-Voltage Curves at Different Irradiances



Current-Voltage Curves at Different Temperatures nos

SUNNY BOY 3000TL-US / 3800TL-US / 4000TL-US / 5000TL-US / 6000TL-US / 7000TL-US / 7700TL-US





Certified

- UL 1741 and 1699B compliant
- Integrated AFCI meets the requirements of NEC 2011 690.11

Innovative

 Secure Power Supply provides daytime power during grid outages

Powerful

- 97,6% maximum efficiency
- Wide input voltage range
- Shade management with OptiTrac Global Peak MPP tracking

Flexible

- Two MPP trackers provide numerous design options
- Extended operating temperature range

SUNNY BOY 3000TL-US / 3800TL-US / 4000TL-US / 5000TL-US / 6000TL-US / 7000TL-US / 7700TL-US



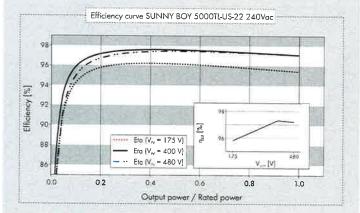
Setting new heights in residential inverter performance

The Sunny Boy 3000TL-US/3800TL-US/4000TL-US/5000TL-US/6000TL-US/7000TL-US/7700TL-US represents the next step in performance for UL certified inverters. Its transformerless design means high efficiency and reduced weight. Maximum power production is derived from wide input voltage and operating temperature ranges. Multiple MPP trackers and OptiTrac™ Global Peak mitigate the effect of shade and allow for installation at challenging sites. The unique Secure Power Supply feature provides daytime power in the event of a grid outage. High performance, flexible design and innovative features make the Sunny Boy TL-US series the first choice among solar professionals.



Technical data	Sunny Boy	3000TL-US	Sunny Boy	3800TL-US	Sunny Boy 4000TL-US		
	208 V AC	240 V AC	208 V AC	240 V AC	208 V AC	240 V AC	
Input (DC)							
Max. usable DC power (@ cos φ = 1)	320	00 W	420	0 W	4200 W		
Max. DC voltage	60	0 V	600 V		600 V		
Rated MPPT voltage range	175 -	480 V	175 -	480 V	175 - 480 V		
MPPT operating voltage range	125 -	125 - 500 V		500 V	125 -	500 V	
Min. DC voltage / start voltage	125 V	/ 150 V	125 V	/ 150 V	125 V	/ 150 V	
Max. operating input current / per MPP tracker	18 A	/15 A	24 A	/15 A		/15 A	
Number of MPP trackers / strings per MPP tracker			2	/2			
Output (AC)							
AC nominal power	300	10 W	3330 W	3840 W	400	0 W	
Max. AC apparent power	300	0 VA	3330 VA	3840 VA	400	0 VA	
Nominal AC voltage / adjustable	208 V / •	240 V / •	208 V / •	240 V / •	208 V / •	240 V / •	
AC voltage range	183 - 229 V	211 - 264 V	183 - 229 V	211 - 264 V	183 - 229 V		
AC grid frequency; range	60 Hz / 59.	.3 - 60.5 Hz	60 Hz / 59.	3 - 60.5 Hz	60 Hz / 59.	3 - 60.5 Hz	
Max. output current		5 A		S A) A	
Power factor (cos φ)		1		1		1	
Output phases / line connections	1,	/2	1 1.	/2	1.	/ 2	
Harmonics		4%		4%		4%	
Efficiency							
Max. efficiency	97.2%	97.6%	97.2%	97.5%	97.2%	97.5%	
CEC efficiency	96.5%	96.5%	96.5%	97.0%	96.5%	97.0%	
Protection devices							
DC disconnection device							
DC reverse-polarity protection							
Ground fault monitoring / Grid monitoring							
AC short circuit protection				1 1 1			
All-pole sensitive residual current monitoring unit							
Arc fault circuit interrupter (AFCI) compliant to UL 1699B							
Protection class / overvoltage category			1/	IV			
General data							
Dimensions (W / H / D) in mm (in)			490 / 519 / 185	(19.3 / 20.5 / 7.3	3)		
DC Disconnect dimensions (W / H / D) in mm (in)			187/297/190				
Packing dimensions (W / H / D) in mm (in)			17/597/266 (
DC Disconnect packing dimensions (W / H / D) in mm (in)			370 / 240 / 280				
Weight / DC Disconnect weight			24 kg (53 lb)				
Packing weight / DC Disconnect packing weight			27 kg (60 lb)				
Operating temperature range		union, _	40 °C +60 °C		'F)		
Noise emission (typical)	\$ 25	dB(A)		dB(A)		dB(A)	
Internal consumption at night		w		W		W	
Topology		rmerless	Transformerless		Transformerless		
Cooling		ection	Convection			ection	
Electronics protection rating		IA 3R	NEMA 3R			A 3R	
Features	7707575	CN 2 5,000			, , , ,		
Secure Power Supply							
Display: graphic							
Interfaces: RS485 / Speedwire/Webconnect	0/	/0	0	10	0.	10	
Warranty: 10 / 15 / 20 years		0/0	•/0		•/0		
Certificates and permits (more available on request)			B, IEEE 1547, FCC F				
NOTE: US in unders abia with over 191							
NOTE: US inverters ship with gray lids		~					
Type designation	SB 3000	IL-US-22	SB 3800	IL-US-22	SB 4000	IL-US-22	





Accessories







• Standard feature O Optional feature — Not available Data at nominal conditions

208 V AC	5000TL-US	Sunny Boy 6000TL-US		Sunny Boy		Sunny Boy	
208 V AC	240 V AC	208 V AC	240 V AC	208 V AC	240 V AC	208 V AC	240 V A
5300 W		6300 W		7300	o w	8000 W	
600 V		60	600 V		v	600 V	
175 -	480 V	210 -	480 V	245 -		270 -	
125 -	500 V	125 -	500 V	125 -	500 V	125 -	
125 V	/ 150 V	125 V,	/ 150 V	125 V /	150 V	125 V /	150 V
30 A	/15 A	30 A	/15 A	30 A /		30 A /	
			2	/2			
4550 W	5000 W	5200 W	6000 W	6000·W	7000 11/	///5011/	7/2014
4550 VA	5000 VA	5200 VA	6000 VA	6000 VA	7000 W	6650 W	7680 W
208 V / •	240 V / •	208 V / •	240 V / ●	208 V / ●	7000 VA	6650 VA	7680 VA
83 - 229·V	211 - 264 V	183 - 229 V	211 - 264 V	183 - 229 V	240 V / • 211 - 264 V	208 V / •	240 V / •
60 Hz / 59.		60 Hz / 59.		60 Hz / 59.3		183 - 229 V 60 Hz / 59.3	211 - 264
22		25		29.2		32	
		1		27.2		32	
1/	12	1/		1/		1/	
< 4		< 2		< 4		< 4	
					~		70
97.2%	97.6%	97.0%	97.4%	96.8%	96.8%	96.8%	97.3%
96.5%	97.0%	96.5%	97.0%	96.5%	96.5%	96.5%	96.5%
				91 = 151x			
				'IV			
			490 / 519 / 185	(19.3 / 20.5 / 7.3)			
				(7.4 / 11.7 / 7.5)			
				24.3 / 23.5 / 10.5)			
				(14.6 / 9.4 / 11.0)			
				/ 3.5 kg (8 lb)			
			27 kg (60 lb)				
- 20	-IR/A)	- 00	-40 °C +60 °C		ID (A)		10/11
< 29 dB(A) < 1 W		< 29 (< 29 d	• • • • • • • • • • • • • • • • • • • •	< 29 d	
Transfor			< 1 W Transformerless			<1	
Convection			п	Transforr Far		Transformerless Fan	
NEMA		NEM		NEMA		NEMA	
		KATE .		•		•	
				•			
		o/ ●/o		•/o,		•/o	

SB 7700TLUS-22

Reviewed for Code
Compliance
Universal Engineerin









Shade management



. .



Secure Power Supply



Flexible communications

A NEW GENERATION OF INNOVATION

The sunny boy tl-us residential series has yet again redefined the category.

Transformerless design

The Sunny Boy 3000TL-US / 3800TL-US / 4000TL-US / 5000TL-US / 6000TL-US / 7000TL-US / 7700TL-US are transformerless inverters, which means owners and installers benefit from high efficiency and lower weight. A wide input voltage range also means the inverters will produce high amounts of power under a number of conditions.

Additionally, transformerless inverters have been shown to be among the safest string inverters on the market. An industry first, the TL-US series has been tested to UL 1741 and UL 1699B and is in compliance with the arc fault requirements of NEC 2011.

Increased energy production

OptiTrac™ Global Peak, SMA's shade-tolerant MPP tracking algorithm, quickly adjusts to changes in solar irradiation, which mitigates the effects of shade and results in higher total power output. And, with two MPP trackers, the TL-US series can ably handle complex roofs with multiple orientations or string lengths.

An extended operating temperature range of -40 °F to +140 °F ensures power is produced

in all types of climates and for longer periods of time than with most traditional string inverters.

Secure Power Supply

One of many unique features of the TL-US residential series is its innovative Secure Power Supply. With most grid-tied inverters, when the grid goes down, so does the solar-powered home. SMA's solution provides daytime energy to a dedicated power outlet during prolonged grid outages, providing homeowners with access to power as long as the sun shines.

Simple installation

As a transformerless inverter, the TL-US residential series is lighter in weight than its transformer-based counterparts, making it easier to lift and transport. A new wall mounting plate features anti-theft security and makes hanging the inverter quick and easy. A simplified DC wiring concept allows the DC disconnect to be used as a wire raceway, saving labor and materials.

The 3800TL-US and 7700TL-US models allow installers to maximize system size and energy production for customers with 100 A and 200 A service panels.

Leading monitoring and control solutions

The new TL-US residential line features more than high performance and a large graphic display. The monitoring and control options provide users with an outstanding degree of flexibility. Multiple communication options allow for a highly controllable inverter and one that can be monitored on Sunny Portal from anywhere on the planet via an Internet connection. Whether communicating through RS485, or SMA's new plug-and-play WebConnect, installers can find an optimal solution to their monitoring needs.

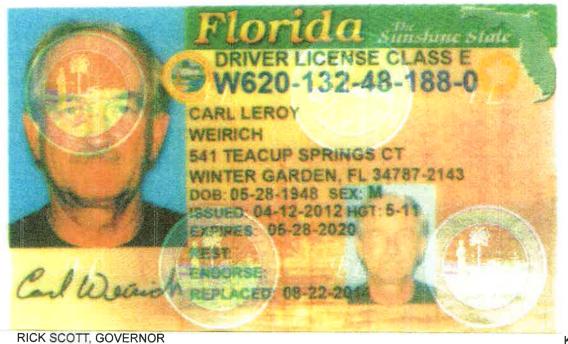
Wide Power Class Range

Whether you're looking for a model to maximize a 100 A service panel or trying to meet the needs of a larger residential PV system, the Sunny Boy TL-US with Secure Power Supply has you covered. Its wide range of power classes—from 3 to 7.7 kW—offers customers the right size for virtually any residential application. The TL-US series is not only the smartest inverter on the planet, it's also the most flexible.



SMA America, LLC

Toll Free +1 888 4 SMA USA www.SMA-America.com



KEN LAWSON, SECRETARY

STATE OF FLORIDA

DEPARTMENT OF BUSINESS AND PROFESSIONAL REGULATION CONSTRUCTION INDUSTRY LICENSING BOARD

LICENSE NUMBER

The SOLAR CONTRACTOR Named below IS CERTIFIED Under the provisions of Chapter 489 FS. Expiration date: AUG 31, 2016

> WEIRICH, CARL L SOLAR-RAY INC. 6007 ANNO AVE ORLANDO

FL 32809





ISSUED: 08/31/2014

DISPLAY AS REQUIRED BY LAW

SEQ # L1408310006481

cott Randolph, Tax Collector

Local Business Tax Receipt

Orange County, Florida

s local business tax receipt is in addition to and not in lieu of any other tax required by law or municipal ordinance. Businesses are subject to regulation of zoning, health and other ful authorities. This receipt is valid from October 1 through September 30 of receipt year. Delinquent penalty is added October 1.

2014

EXPIRES

9/30/2015

3501-0561833

3501 SOLAR ENERGY PRODUC

\$30.00

EMPLOYEE 3

TOTAL TAX PREVIOUSLY PAID TOTAL DUE

\$30.00 \$30.00 \$0.00

SOLAR RAY INC

SOLAR RAY SOLAR RAY INC 6007 ANNO AVE ORLANDO FL 32809

6007 ANNO AVE (MOBILE) U - ORLANDO, 32809



JEFF ATWATER CHIEF FINANCIAL OFFICER

STATE OF FLORIDA DEPARTMENT OF FINANCIAL SERVICES DIVISION OF WORKERS' COMPENSATION

** CERTIFICATE OF ELECTION TO BE EXEMPT FROM FLORIDA WORKERS' COMPENSATION LAW **

CONSTRUCTION INDUSTRY EXEMPTION

This certifies that the individual listed below has elected to be exempt from Florida Workers' Compensation law.

EFFECTIVE DATE: 5/9/2014

EXPIRATION DATE: 5/8/2016

PERSON: WEIRICH

CARL

L

FEIN:

550844985

BUSINESS NAME AND ADDRESS:

SOLAR RAY INC

2014 PAGE AVE

ORLANDO

32806

SCOPES OF BUSINESS OR TRADE:

MACHINERY OR EQUIPMENT ERECTIO

PLUMBING NOC AND DRIVERS

ELECTRICAL WIRING WITHIN BUIL

ROOFING - ALL KINDS AND DRIVER

used to Chapter 440.08(14), F.S., an officer of a corporation who sower benefits or compensation under this chapter. Pursuant to be business or trade field on the notice of election to be exempt, ion to be exempt, shall be subject to revocation if, at any time at loate no longer meets the requirements of this section for lesues on named on this certificate to meet the requirements of the

DFS-F2-DWC-252 CERTIFICATE OF ELECTION TO BE EXEMPT REVISED 07-12

QUESTIONS? (850)413-1609



CERTIFICATE OF LIABILITY INSURANCE

SOLAR-1

OP ID: CS

DATE (MM/DD/YYYY) 04/07/2015

THIS CERTIFICATE IS ISSUED AS A MATTER OF INFORMATION ONLY AND CONFERS NO RIGHTS UPON THE CERTIFICATE HOLDER. THIS CERTIFICATE DOES NOT AFFIRMATIVELY OR NEGATIVELY AMEND, EXTEND OR ALTER THE COVERAGE AFFORDED BY THE POLICIES BELOW. THIS CERTIFICATE OF INSURANCE DOES NOT CONSTITUTE A CONTRACT BETWEEN THE ISSUING INSURER(S), AUTHORIZED REPRESENTATIVE OR PRODUCER, AND THE CERTIFICATE HOLDER.

IMPORTANT: If the certificate holder is an ADDITIONAL INSURED, the policy(ies) must be endorsed. If SUBROGATION IS WAIVED, subject to the terms and conditions of the policy, certain policies may require an endorsement. A statement on this certificate does not confer rights to the

	are mereal in floa of odolf chaols	sement(s).			
PRODUCER	and Risk Management		CONTACT Marty Smith		
of Florida	, LLC		PHONE (A/C, No. Ext): 321-214-1990	21-710-2501	
Longwood	n Oak Centre Drive d, FL 32750		E-MAIL ADDRESS: martys@irmtoday.com	, Viscitus P	
David Russell Curry		INSURER(S) AFFORDING CO	OVERAGE	NAIC #	
			INSURER A : Maxum Indemnity Com	pany	
INSURED	Solar-Ray, Inc.		INSURER B : Old Dominion Insurance	e Company	40231
	PO Box 560481 Orlando, FL 32806		INSURER C: Nautilus Insurance Co	itilus Insurance Co	
			INSURER D :		
			INSURER E :		
			INSURER F :		
COVERA		TIFICATE NUMBER:	REVIS	SION NUMBER:	
INDICAL	ED NOTWITHSTANDING ANY RE	QUIREMENT. FERM OR CONDITIO	AVE BEEN ISSUED TO THE INSURED NAM N OF ANY CONTRACT OR OTHER DOCUM	MED ABOVE FOR THE F	O WHICH THIS
EVOLUS	IONS AND CONDITIONS OF SUCH F	PERTAIN, THE INSURANCE AFFOR POLICIES, LIMITS SHOWN MAY HAV	DED BY THE POLICIES DESCRIBED HER E BEEN REDUCED BY PAID CLAIMS.	EIN IS SUBJECT TO AL	L THE TERMS,
INSR		ADDI CIIDO			

LTR		TYPE OF INSURANCE	INSD WVI		POLICY EFF (MM/DD/YYYY)	POLICY EXP (MM/DD/YYYY)	LIMITS		
A	X	CLAIMS-MADE X OCCUR		BDG3005778-01		04/24/2015	EACH OCCURRENCE DAMAGE TO RENTED PREMISES (Ea occurrence)	\$	1,000,000 100,000
1							MED EXP (Any one person)	\$	1,000
1							PERSONAL & ADV INJURY	\$	1,000,000
1	GEN	I'L AGGREGATE LIMIT APPLIES PER:					GENERAL AGGREGATE	\$	2,000,000
		POLICY PRO- JECT LOC					PRODUCTS - COMP/OP AGG	\$	2,000,000
-		OTHER:						\$	
١.		OMOBILE LIABILITY					COMBINED SINGLE LIMIT (Ea accident)	\$	1,000,000
Α	X	ANY AUTO ALL OWNED SCHEDULED		B1T6267N	05/08/2014	05/08/2015	BODILY INJURY (Per person)	\$	
		AUTOS AUTOS					BODILY INJURY (Per accident)	\$	
		HIRED AUTOS NON-OWNED AUTOS					PROPERTY DAMAGE (Per accident)	\$	
								\$	
		UMBRELLA LIAB X OCCUR					EACH OCCURRENCE	\$	1,000,000
C	X	EXCESS LIAB CLAIMS-MADE		AN017781	11/11/2014	11/11/2015	AGGREGATE	\$	1,000,000
		DED RETENTION \$						\$	1,000,000
		KERS COMPENSATION EMPLOYERS' LIABILITY					PER OTH- STATUTE ER	_	
	ANY I	PROPRIETOR/PARTNER/EXECUTIVE T/N	N/A				E.L. EACH ACCIDENT	\$	
	(Man	DER/MEMBER EXCLUDED? datory in NH)	N/A				E L DISEASE - EA EMPLOYEE		
	If yes	describe under CRIPTION OF OPERATIONS below					E.L. DISEASE - POLICY LIMIT		
								Ψ	
DESC	CRIPTI	ON OF OPERATIONS / LOCATIONS / VEHICI	LES (ACOR	D 101, Additional Remarks Sched	lule, may be attached if mor	e space is requir	ed)		
CEF	RTIF	CATE HOLDER			CANCELLATION				
		City of Belle Isle		BELLEIS	SHOULD ANY OF 1	I DATE THE	ESCRIBED POLICIES BE CARREDF, NOTICE WILL E	ANCELI BE DE	LED BEFORE LIVERED IN

ACORD 25 (2014/01)

City of Belle Isle 1600 Nela Avenue Belle Isle, FL 32809

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AUTHORIZED REPRESENTATIVE

W. 874/3